

UNITED STATES
DEPARTMENT OF THE INTERIOR
GEOLOGICAL SURVEY

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DOCUMENTATION OF PROGRAMS THAT COMPUTE

- 1) STATIC TILTS FOR A SPATIALLY VARIABLE SLIP DISTRIBUTION, AND
- 2) QUASI-STATIC TILTS PRODUCED BY AN EXPANDING DISLOCATION LOOP
WITH A SPATIALLY VARIABLE SLIP DISTRIBUTION

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Open-File Report #76-578

This report is preliminary and has not been
edited or reviewed for conformity with Geological
Survey standards and nomenclature.

Note: Some of the pages in this report may be difficult to read. This is
the best copy that can be made from the original.

OCT 11 1976

ABSTRACT

The material in this report is concerned with the effects of a vertically oriented rectangular dislocation loop on the tilts observed at the free surface of an elastic half-space. Part I examines the effect of a spatially variable static strike-slip distribution across the slip surface. The tilt components as a function of distance parallel, or perpendicular, to the strike of the slip surface are displayed for different slip-versus-distance profiles. Part II examines the effect of spatially and temporally variable slip distributions across the dislocation loop on the quasi-static tilts at the free surface of an elastic half space. The model discussed in part II may be used to generate theoretical tilt versus time curves produced by creep events.

INTRODUCTION:

Program RCTNGL computes the tilt-versus-distance profiles observed for a variable strike-slip distribution across a slip surface. The model assumes a vertically oriented rectangular dislocation loop embedded in an elastic half-space. The distance axis of the profile may be parallel or perpendicular to the strike of the slip surface. The position of the slip surface relative to the position of the profile is arbitrary, and various slip distributions may be modelled by changing a few lines in the program.

Program SLPPRP also assumes a vertically oriented rectangular dislocation loop embedded in an elastic half-space to generate a quasi-static tilt-time profile produced by spatially and temporally variable slip distributions. This program may be used to model creep-related tilt changes; and provides a self-consistent method of separating the tilt changes produced by propagation effects of the boundaries of the slip surface from the tilt changes produced by time variations in the slip distribution across the slip surface.

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DOCUMENTATION OF PROGRAM RCTNGL

PART I

DOCUMENTATION FOR PROGRAM RCTNGL

INTRODUCTION:

The tilts, produced by a vertically oriented rectangular dislocation loop, observed at the free surface of an elastic half-space depend upon the source-station geometry, the amount and type of slip, and the slip distribution. This program uses the expressions for tilt given in Press (1965), and allows the user to select the profile desired and the distribution of slip. The output consists of the tilt components and tilt amplitude and azimuth versus distance. With this program, the user may, for example, examine the dependence of the surface tilts on the spatial frequency of the slip distribution.

INPUT:

The geometry and notation assumed are shown in Figures 1.1 and 1.2, and definitions of the parameters used are provided in Appendix A. Although this program assumes strike slip displacement, dip-slip displacement may be used by changing the expressions in subroutine TILT to conform to those given in Press (1965). This program also assumes a cosinusoidal slip distribution with spatial frequencies FREQX1 in the X1 direction and FREQX3 in the X3 direction. If other slip distributions are desired, lines 57 - 59 in the main program may be altered. For example, if line 59 is deleted, the slip will be alternately right- and left-lateral across the slip surface (if line 59 is retained, the absolute magnitude of the cosinusoidal slip distribution is computed). If, for example, lines 57 through 59 are changed to:

```
ALPHA = + .5* SQRT (((I-(N2/2.))**2)+((J-(N1/2.))**2))
```

```
U = UMAX * (-1. + EXP (ALPHA))
```

the slip distribution will increase exponentially away from the center of the slip zone. Or, if lines 57-59 are changed to:

```
ALPHA = -.5* SQRT (((I-(N2/2.))**2)+((5-(N1/2.))**2))
```

```
U = -UMAX * ((N2 + N1)/2.)* EXP (ALPHA)
```

the slip distribution will decrease exponentially away from the center of the slip zone. (The value of .5 and the pre-exponential factor were arbitrarily chosen to scale the slip magnitude.) The subrectangles are labelled as shown in Figure 1.3. Notice that the slip is constant across each subrectangle, but may vary from subrectangle to subrectangle.

The program is intended for use on the LBL 6600 B or C machine and the Tektronix 4010-1 terminal. It requires 40K of core and may be accessed using

```
^LOAD, RCTNGL, MCHUGH .
```

It will automatically link to the appropriate plotting subroutines, and the ^LOAD command may be followed by a ^RUN. The computer responds as follows:

- 1) 1 = plot vs. X1, 2 = plot vs. X2

Enter 1 or 2 to select the profile desired.

- 2) Specify initial and final points of plot.

Enter the beginning and end points of the profile in kilometers.

- 3) Specify value of {X1, X2} that profile is computed for.

Enter the X1 (X2) position of the X2 (X1) profile in kilometers.

- 4) Specify C1X1FN, C1X3FN, C2X3FN, C3X1FN

Enter the 4 endpoints of the slip zone.

- 5) Specify number of points in profile,
Number of columns and rows,
Spatial frequency of slip in X1 direction,
Spatial frequency of slip in X3 direction
And maximum slip

Enter the 5 quantities required.

- 6) Specify angle of fault to NS axis, in degrees.

Enter the angle between the strike of the slip surface and north.

OUTPUT:

- 1) MIN/MAX values of EW component (numerical values)
MIN/MAX values of NS component (numerical values)
MIN/MAX values of amplitude (numerical values)
MIN/MAX values of azimuth (numerical values)

(Note tilt amplitudes are in microradians azimuth in degrees)

The following are plots of the EW and NS components of tilt
and the tilt amplitude and azimuth (measured clockwise from
north).

0 = Re-Start, 1 = Continue

Entering a zero causes the program to start at step (1). In the
Input section, a 1 causes the program to continue.

- 2) Write plot title, 80 characters

Enter up to 80 alphanumeric characters.

- 3) Set horizontal scale? Y or N (= Blank)

Entering a Y causes the computer to respond:

MIN/MAX X values

Entering an N or (blank) causes the horizontal scale to terminate at
the endpoints selected in part 2 of Input.

4) Set vertical scale? Y or N (= Blank)

The procedure is the same as in part 3 above.

The output consists of a sequence of plots of the EW tilt component (equivalent to $\frac{\partial W}{\partial X_2}$ if theta equals zero), the NS component (equivalent to $\frac{\partial W}{\partial X_1}$ if theta equals zero), the tilt amplitude, and the tilt azimuth. The profiles are parallel to the X1 or X2 directions as specified in part 1 in Input.

RESULTS:

Examples of the variation in tilt for the profiles and slip distributions indicated are shown in the 'Examples' section. The examples are shown on pages 1-7 through 1-38. The major points to be noted are that 1) as the spatial frequency of slip is increased the surface tilts approach those expected for constant displacement across the slip zone and 2) as the slip distribution is confined to some small region of the slip surface, the tilts approach those expected for a point source at the region of maximum slip. In principle, at least, the surface tilt field may provide some information about spatial variations in the slip distribution.

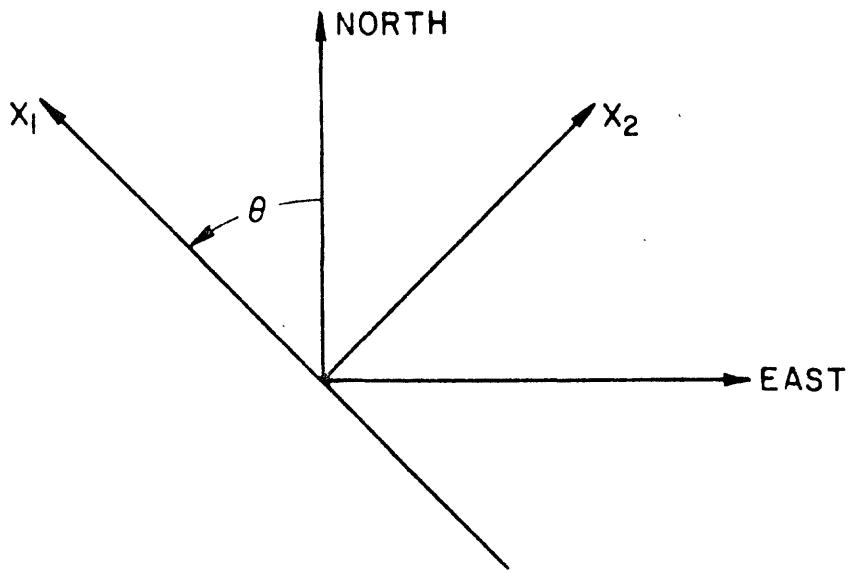


FIG. I.1 SLIP SURFACE ORIENTATION RELATIVE TO OBSERVER

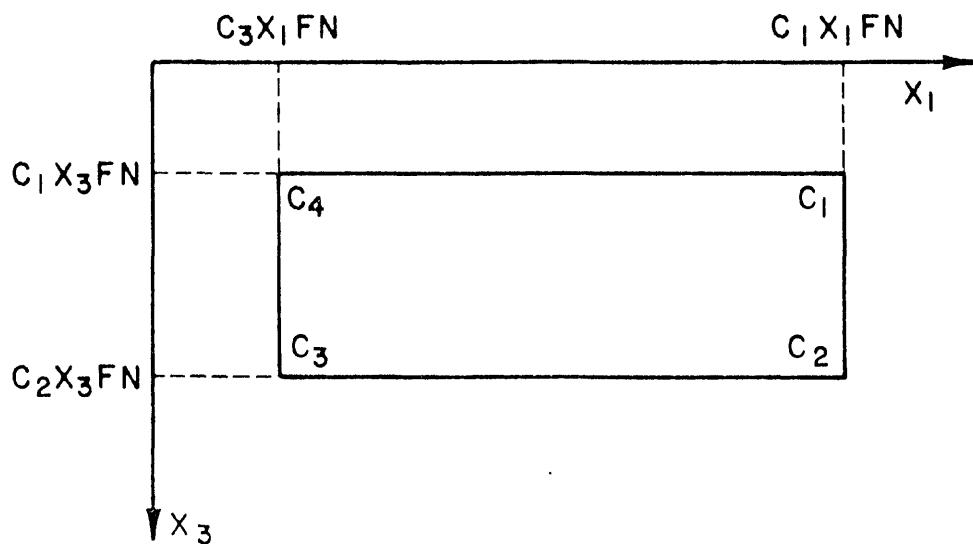


FIG. I.2 POSITION OF SLIP SURFACE BOUNDARIES

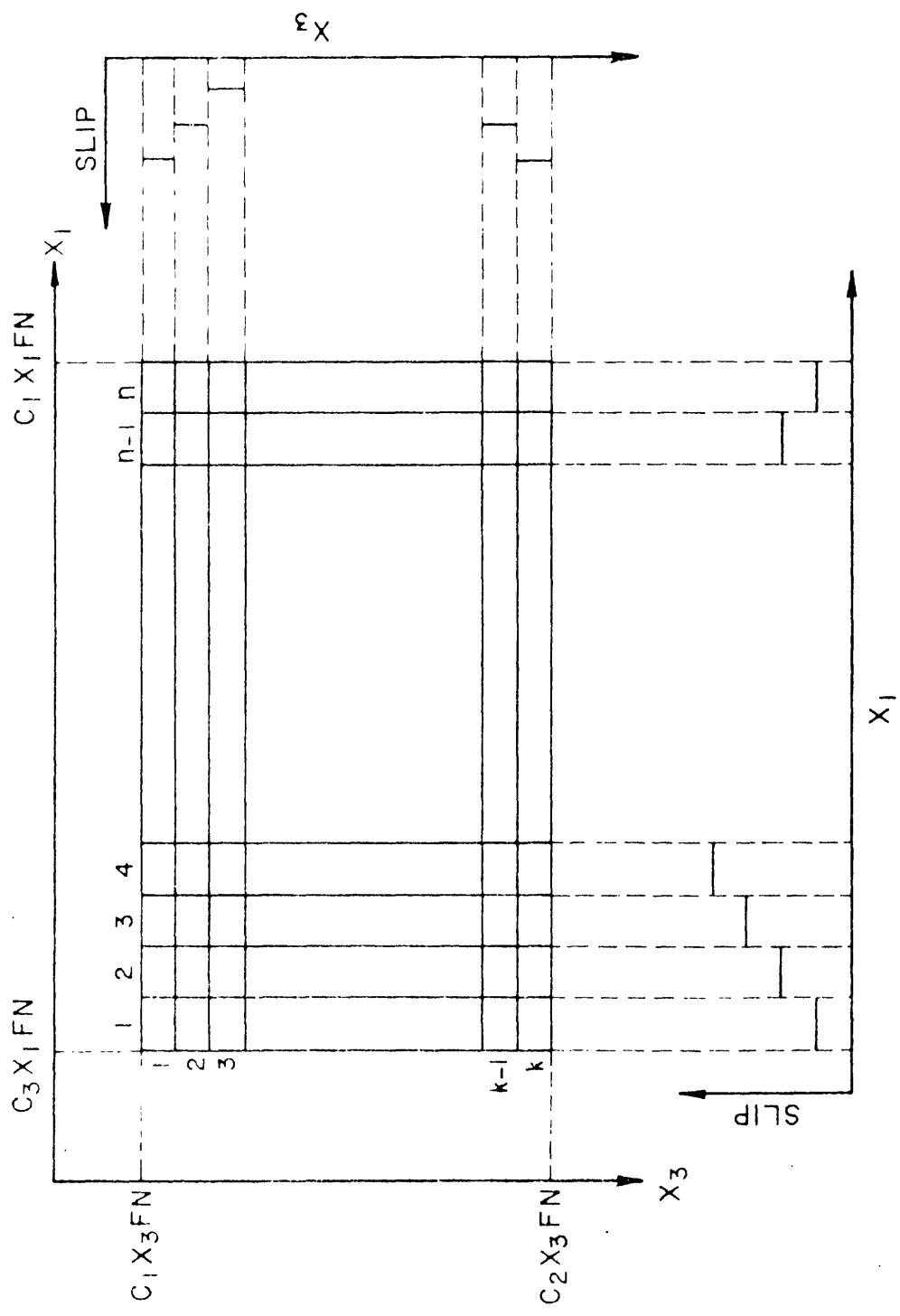


FIG. I 3 LABELLING OF SUBRECTANGLES AND A HYPOTHETICAL SLIP DISTRIBUTION

APPENDIX A

Parameters used in RCTNGL:

IFLAG - determines whether tilt profile is parallel to the X1 or X2 the axis

BEGIN, END - endpoints of the tilt profile

CNSTNT - position of profile

C1X1FN, C1X3FN, C2X3FN, C3X1FN - coordinates of slip surface

M - number of points in tilt profile

N1, N2 - number of columns and rows respectively that comprise slip surface

FREQX1, FREQX3 - spatial frequencies in X1 and X3 directions respectively

UMAX - maximum displacement on slip surface

Theta - angle between strike of fault and north

EXAMPLES OF RCTNGL

RCTNGL

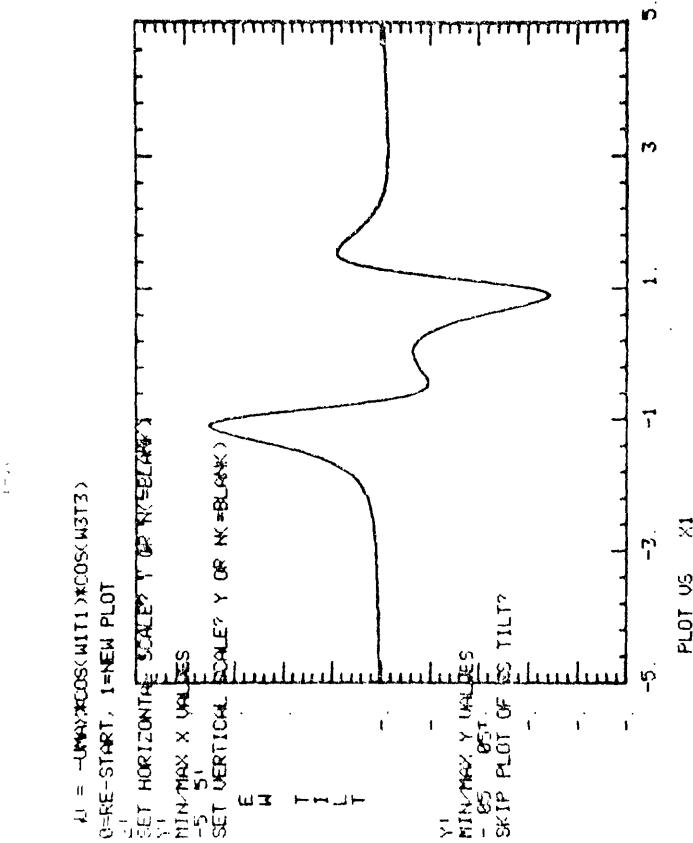
Cosinusoidal Slip Distribution

The slip distribution across the slip zone is specified in lines 57-59 of the documentation for RCTNGL (Page 1-39). Note that the absolute value of the slip is used in these examples.

```

~RUN!
1 PLOT US. X1, 2=PLOT US. X2
      MIN/MAX Y VALUES
      -85   85
SPECIFY INITIAL AND FINAL POINTS OF PLOT
-5 5
SPECIFY VALUE OF X2 THAT PROFILE IS COMPUTED FOR
51
SPECIFY C1X1FH,C1X2FN,C2X3FN,C3X1FH
1 0 1 -1
SPECIFY NUMBER OF POINTS IN PROFILE,
NUMBER OF COLUMNS AND ROWS,
SPATIAL FREQUENCY OF SLIP IN X1 DIRECTION,
SPATIAL FREQUENCY OF SLIP IN X3 DIRECTION,
ACI AS A HARMONIC SLIP
2 3 2 5 6 11
SPECIFY ANGLE OF PLOT TO NS AXIS, IN DEGREES
45
MIN SPAN VALUES OF EW COMPONENT -3 423E-02 3 597E-02
MIN SPAN VALUES OF NS COMPONENT -3 597E-02 3 423E-02
MIN SPAN VALUES OF AMPLITUDE 7 173E-04 3 781E-02
MIN SPAN VALUES OF AZIMUTH 5 975 358 148
(NOTE: TILT AMPLITUDES ARE IN MICRODEGREES)
AZIMUTH IN DEGREES)
THE FOLLOWING ARE PLOTS OF THE EW AND NS
COMPONENTS OF TILT, AND THE TILT AMPLITUDE
AND AZIMUTH (MEASURED CLOCKWISE FROM NORTH),
6=RE-START, 1=CONTINUE
1
1 PLOT TITLE FOR CHARACTERS
U=-1MAXX*COS(W1)*COS(W2T3),
SET HORIZONTAL SCALE? Y OR N=BLANK,
Y1
MIN/MAX X VALUES
-5 5
SET VERTICAL SCALE? Y OR N=BLANK
5
PLOT US. X1

```



1 - 11

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PLOT

NET HORIZONTAL SCALE?

INTRODUCTION

VERTICES SCALE? Y C

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1

1

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S33

skip plot cell

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1

1

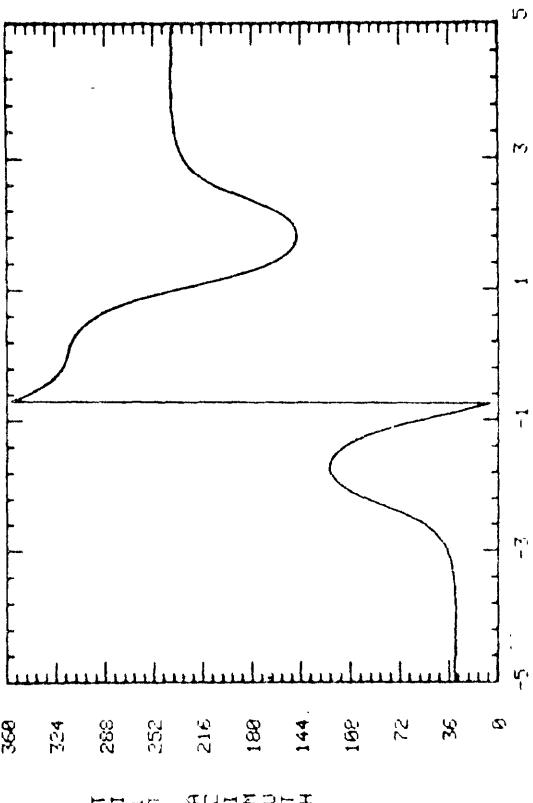
卷之三

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PLOT US

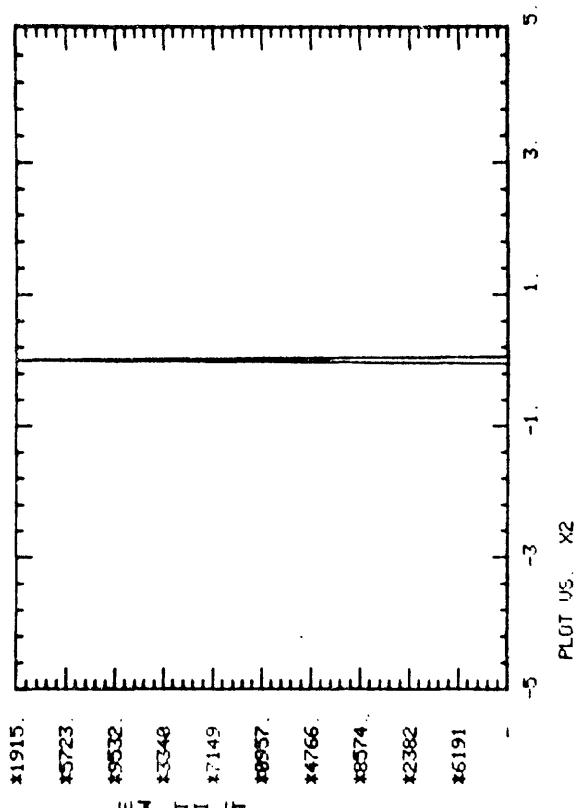
$y = -\text{MAX}(X) \cdot \cos(W \cdot X \cdot T3)$
 0-RE-START. 1-NEW PLOT
 SET HORIZONTAL SCALE? Y OR N =BLANK
 MIN MAX X VALUES
 T I L F A M P L I T U D E
 SET VERTICAL SCALE? Y OR N =BLANK
 MIN MAX Y VALUES
 0 301 S KIP PLOT OF SET ZEROEDIN?

$U = -1.0 \times \cos(\omega_1 t) \cos(\omega_2 t)$
 1=PLOT US X1, 2= PLOT US X2 Slip Plot of EW TILT?
 SPECIFY INITIAL AND FINAL POINTS OF PLOT
 -5 51
 SPECIFY VALUE OF X1 THAT PROFILE IS COMPUTED FOR
 E1
 SPECIFY C1X1FN,C1X3FN,C2X3FN
 1 61 -11
 SPECIFY NUMBER OF POINTS IN PROFILE,
 NUMBER OF COLUMNS AND ROWS,
 SPATIAL FREQUENCY OF SLIP IN X1 DIRECTION,
 SPATIAL FREQUENCY OF SLIP IN X3 DIRECTION,
 AND MAXIMUM SLIP
 288 28 28 4 1,
 SPECIFY ANGLE OF FAULT TO NS AXIS, IN DEGREES
 01
 MIN MAX VALUES OF EW COMPONENT -1 893E-81 3 412E+10
 MIN MAX VALUES OF NS COMPONENT -2 60E-82 1 363E+11
 MIN MAX VALUES OF AMPLITUDE 5 454E-84 1 407E+11
 MIN MAX VALUES OF AZIMUTH 652 359 240
 NOTE: TILT AMPLITUDES ARE IN MICROGRADS
 AZIMUTH IN DEGREES,
 THE FOLLOWING ARE PLOTS OF THE EW AND NS
 COMPONENTS OF TILT, AND THE TILT AMPLITUDE
 AND AZIMUTH (MEASURED CLOCKWISE FROM NORTH,
 E= E-SOUTH, 1=CONTINUE
 1
 SPECIE PLOT TITLE, 80 CHARACTERS
 U = -485.0MAXCOS(W1)*COS(W2)*X*23X3
 SET HORIZONTAL SCALE? Y OR N =BLANK
 ?1
 MIN MAX X VALUES
 -5 51
 SET VERTICAL SCALE? Y OR N =E1H4
 ?1
 PLOT :5 .1

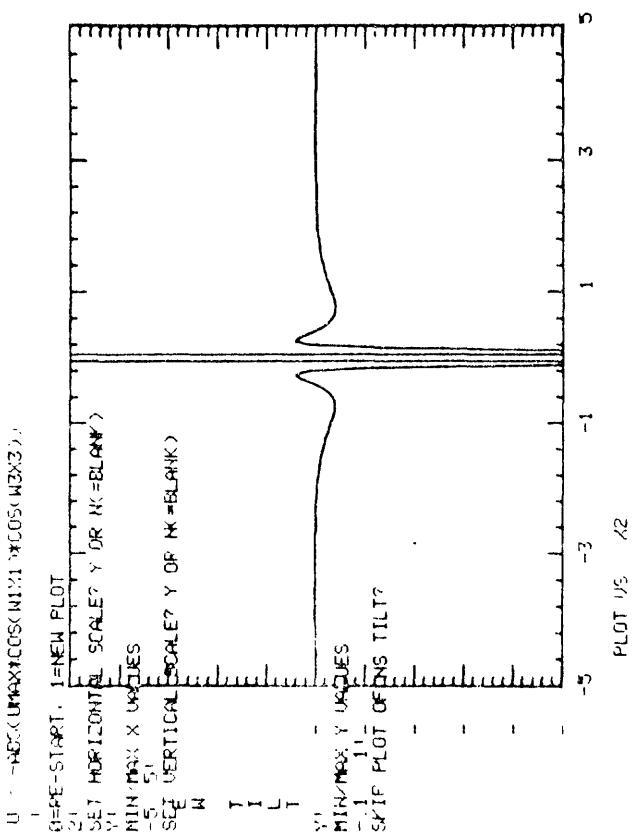
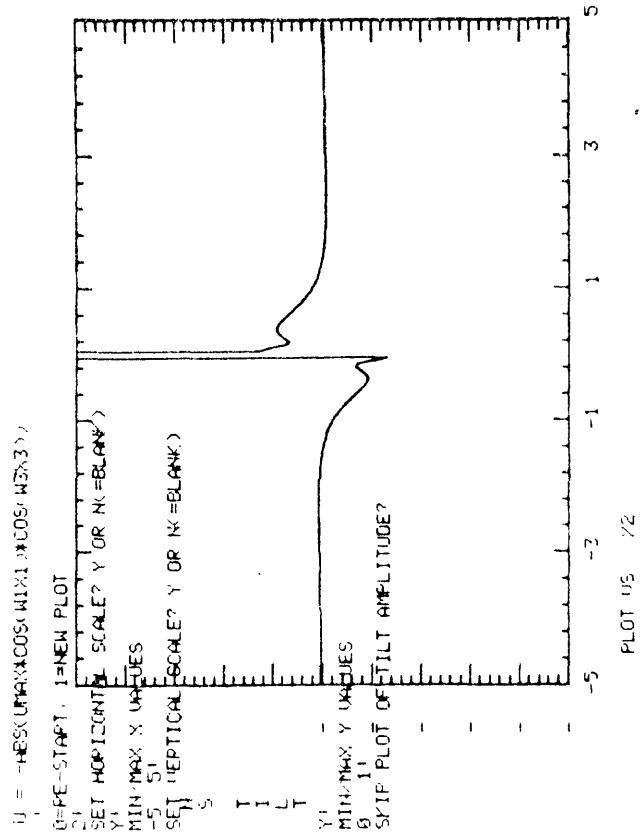


1-15

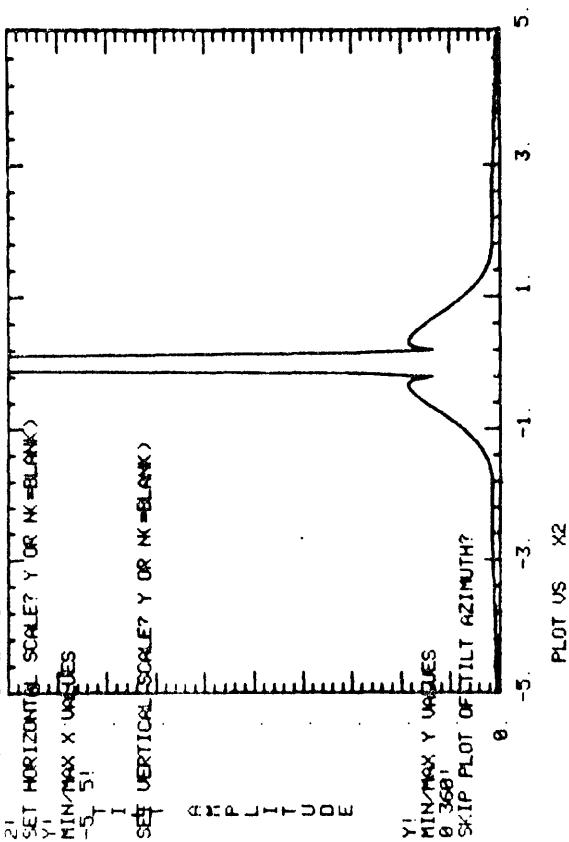
$$U = -\text{ABS}(\text{UNPK}(X1) \text{COS}(W3X3))$$



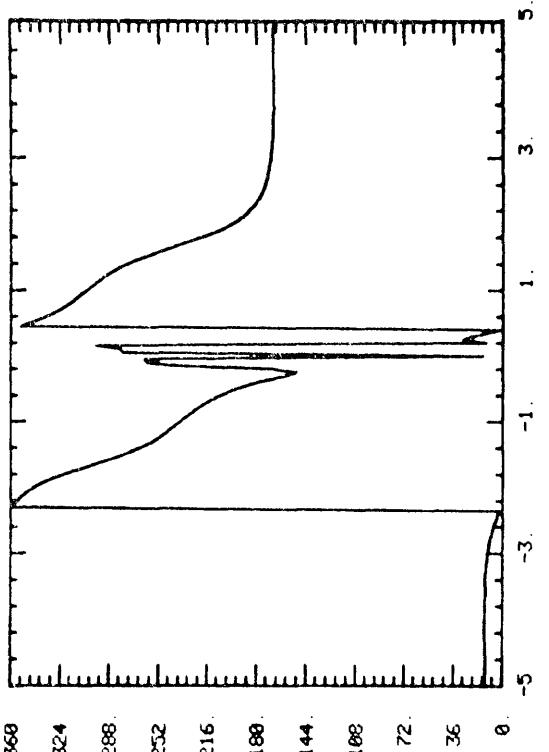
```
B-RE-START, 1-NEW PLOT  
1!  
SET HORIZONTAL SCALE? Y OR NK=BLANK  
Y!  
MIN MAX X VALUES  
-5 5!  
SET VERTICAL SCALE? Y OR NK=BLANK  
Y!  
MIN MAX Y VALUES  
-1 1!  
SKIP PLOT OF EU TILT?
```



1-19
 U = -ABSK(UMAX*COS(W1X1)*COS(W3X3))
 0=RE-START, 1=NEW PLOT
 SET HORIZONTAL SCALE? Y OR N-BLANK
 Y1 MIN/MAX X VALUES
 -5 5.
 1 SET VERTICAL SCALE? Y OR N-BLANK
 A
 M P
 L
 I T U D E
 E



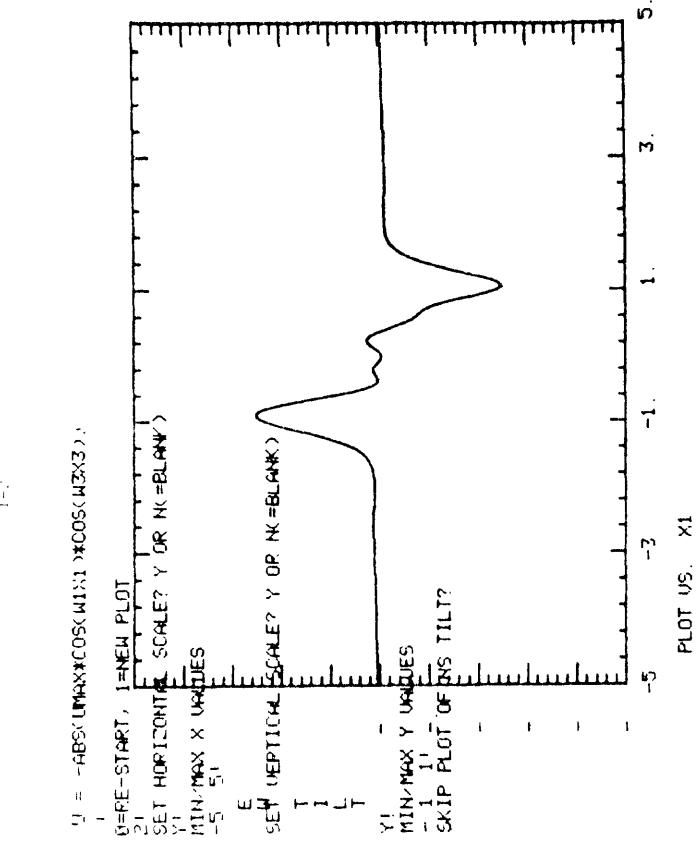
1-20
 U = -ABSK(UMAX*COS(W1X1)*COS(W3X3))
 368 324 288 252 216 180 144 108 72 36 0.
 T I L T A Z I M U T H
 PLOT US. X2



```

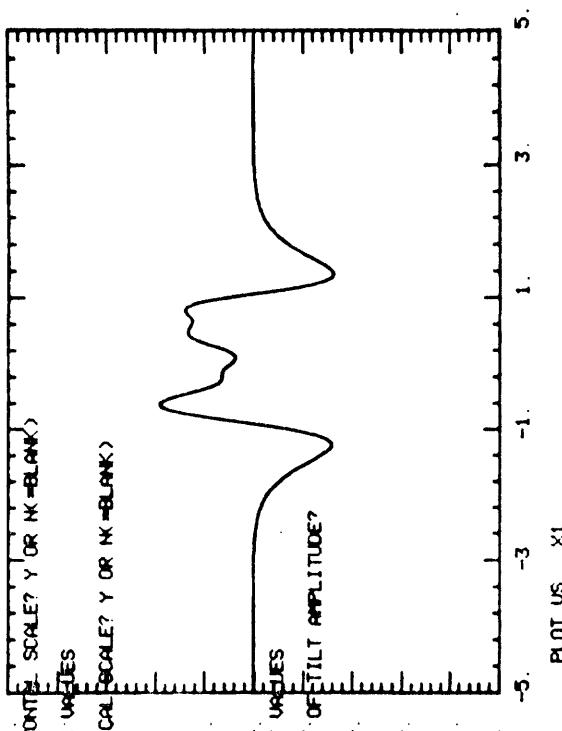
0=RE-START, 1=NEW PLOT
0! 1=PLOT US X1, 2=PLOT VS. X2
1! SPECIFY INITIAL AND FINAL POINTS OF PLOT
-5 .5!
SPECIFY VALUE OF X2 THAT PROFILE IS COMPUTED FOR
5!
SPECIFY C1X1FN,C1X3FN,C2X3FN,C3X1FN
1.0 .1!
SPECIFY NUMBER OF POINTS IN PROFILE,
NUMBER OF COLUMNS AND ROWS,
SPECIFY FREQUENCY OF SLIP IN X1 DIRECTION,
SPECIFY FREQUENCY OF SLIP IN X3 DIRECTION,
AND MAXIMUM SLIP
200 1E-1 2 .6 .1!
SPECIFY ANGLE OF FAULT TO NS AXIS, IN DEGREES
0!
MIN /MAX VALUES OF EH COMPONENT -4.974E-02 5.024E-02
MIN /MAX VALUES OF NS COMPONENT -3.221E-02 3.889E-02
MIN /MAX VALUES OF AMPLITUDE 9.266E-04 5.067E-02
MIN /MAX VALUES OF AZIMUTH .945 357.378
<NOTE TILT AMPLITUDES ARE IN MICRORADIAN>
AZIMUTH (IN DEGREES)
THE FOLLOWING ARE PLOTS OF THE EH AND NS
COMPONENTS OF TILT, AND THE TILT AMPLITUDE
AND AZIMUTH (MEASURED CLOCKWISE FROM NORTH).
0=RE-START, 1=CONTINUE
1!
WRITE PLUT TITLE, 80 CHARACTERS
U = -ABS(UMAX*X*COS(W1*X1)*COS(W3*X3))
SET HORIZONTAL SCALE? Y OR N=BLANK?
Y!
MIN/MAX X VALUES
-5 .5!
SET VERTICAL SCALE? Y OR N=BLANK?
E!
SET HORIZONTAL SCALE? Y OR N=BLANK?
Y!
MIN/MAX Y VALUES
-1 1!
SET PLOT OF NS TILT?
-!
SET PLOT OF EW TILT?
-!
PLOT US. X1
MIN/MAX X VALUES
-5 .5!

```



1-23

U = -485(X1MAX*X1)*COS(X1)*COS(X3))
0=RE-START, 1=NEW PLOT
2 SET HORIZONTAL SCALE? Y OR NK=BLANK?
Y1 MIN/MAX X VALUES
-5 5!
SET VERTICAL SCALE? Y OR NK=BLANK?
Y1 MIN/MAX Y VALUES
0 1.
SKIP PLOT OFF/FILT AMPLITUDE?



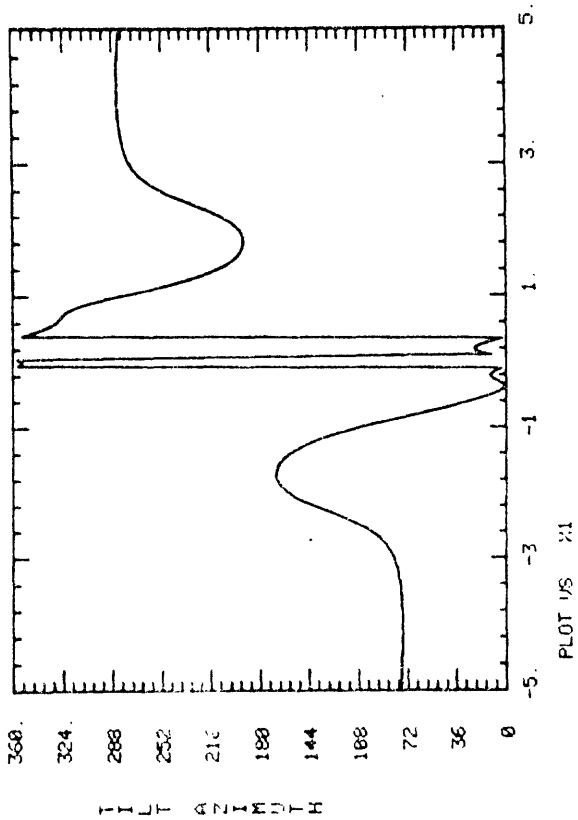
1-24

U = -485(X1MAX*X1)*COS(X1)*COS(X3))
0=RE-START, 1=NEW PLOT
2 SET HORIZONTAL SCALE? Y OR NK=BLANK?
Y1 MIN/MAX X VALUES
-5 5!
SET VERTICAL SCALE? Y OR NK=BLANK?
Y1 MIN/MAX Y VALUES
0 1.
SKIP PLOT OFF/FILT AZIMUTH?



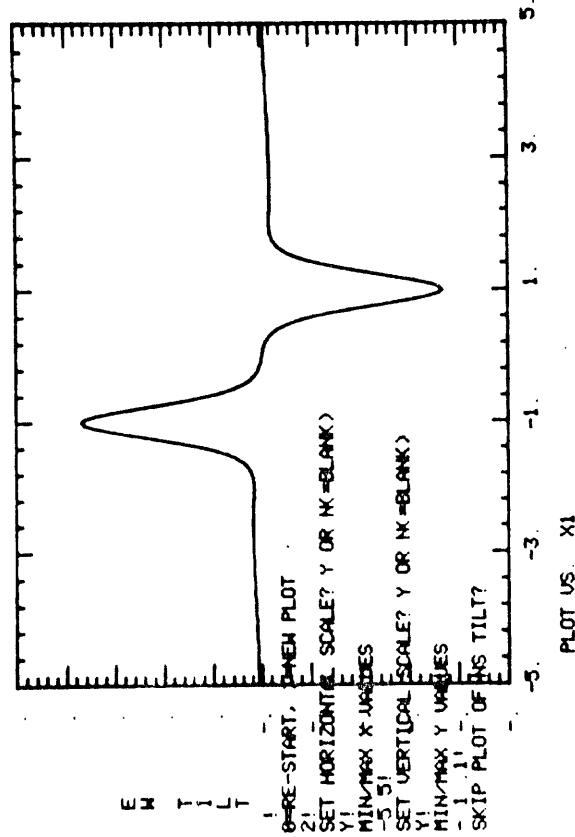
$U = -HBSC(\text{UMAX} * \text{COS}(W1X1) * \text{COS}(W3X3))$

0=RE-START, 1=NEW PLOT
0! SET VERTICAL SCALE? Y OR N=N-BLANK?
1=PLOT US X1, 2=PLOT US X2
Y MIN-MAX Y VALUES
1! SPECIFY INITIAL AND FINAL POINTS OF PLOT
-5 5! SKIP PLOT OF EW TILT?
SPECIFY VALUE OF X2 THAT PROFILE IS COMPUTED FOR
5!
SPECIFY C1X1FN,C1X3FN,C2X3FN,C3X1FN
1 6 1 -1!
SPECIFY NUMBER OF POINTS IN PROFILE,
NUMBER OF COLUMNS AND ROWS,
SPATIAL FREQUENCY OF SLIP IN X1 DIRECTION,
SPATIAL FREQUENCY OF SLIP IN X3 DIRECTION,
AND MAXIMUM SLIP
288 1 1 6 6!
SPECIFY ANGLE OF FAULT TO NS AXIS, IN DEGREES
0!
MIN /MAX VALUES OF EW COMPONENT -7.383E-02 7.383E-02
MIN /MAX VALUES OF NS COMPONENT -4.674E-02 4.674E-02
MIN /MAX VALUES OF AMPLITUDE 1.468E-03 7.384E-02
MIN /MAX VALUES OF AZIMUTH 719 719
(NOTE: TILT AMPLITUDES ARE IN MICRORADIAN)
AZIMUTH IN DEGREES
THE FOLLOWING ARE PLOTS OF THE EW AND NS
COMPONENTS OF TILT, AND THE TILT AMPLITUDE
AND AZIMUTH (MEASURED CLOCKWISE FROM NORTH)
0=PE-START, 1=CONTINUE
1!
WRITE PLOT TITLE, 80 CHARACTERS
PENTAGON/UNIFORM SLIP!
SET HORIZONTAL SCALE? Y OR N=N-BLANK?
Y!
MIN-MAX X VALUES



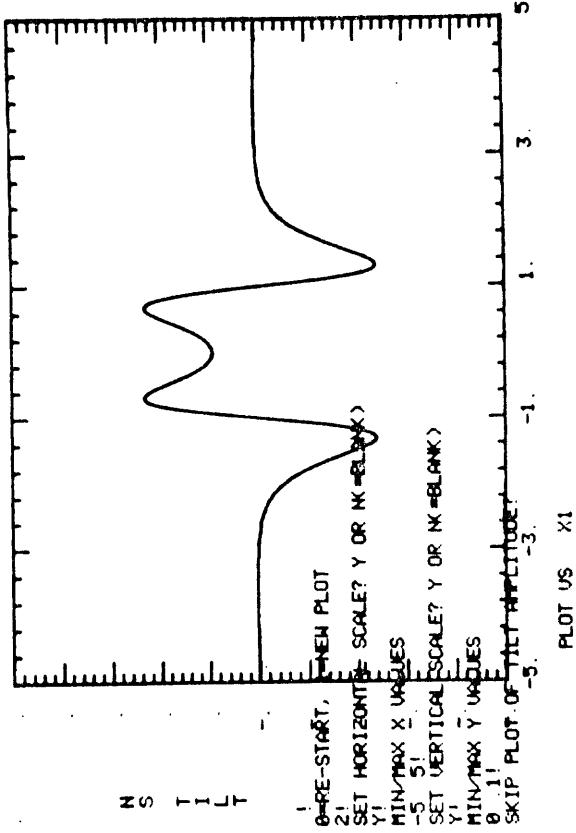
1-27

RECTANGLE/UNIFORM SLIP

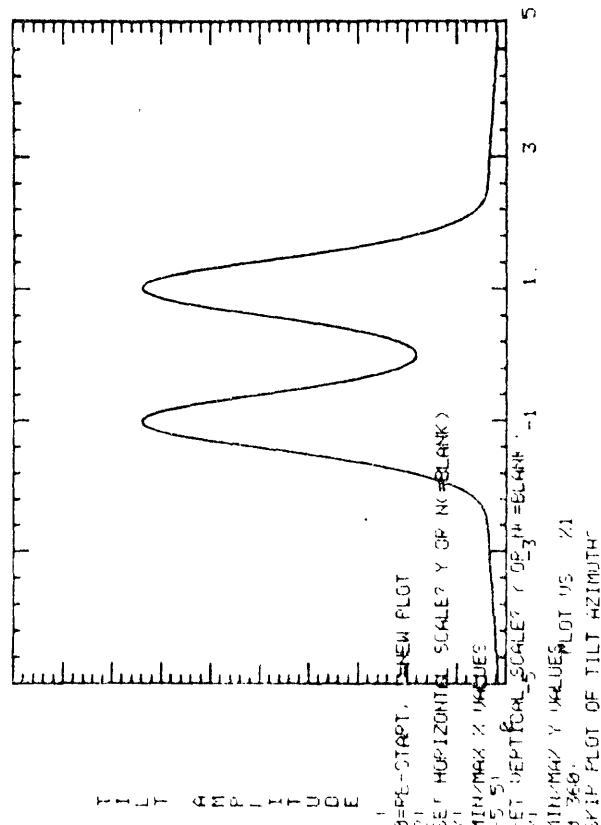


1-28

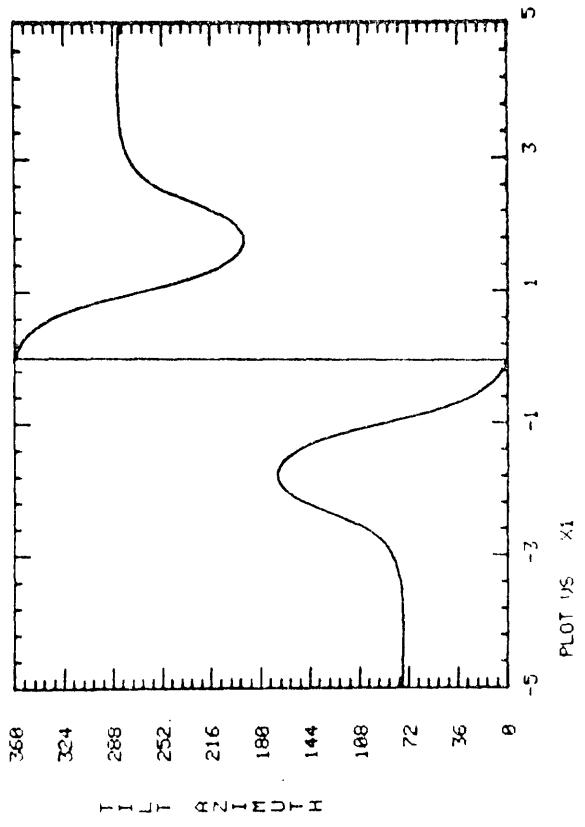
RECTANGLE/UNIFORM SLIP



RECTANGLE UNIFORM SLIP



RECTANGLE UNIFORM SLIP



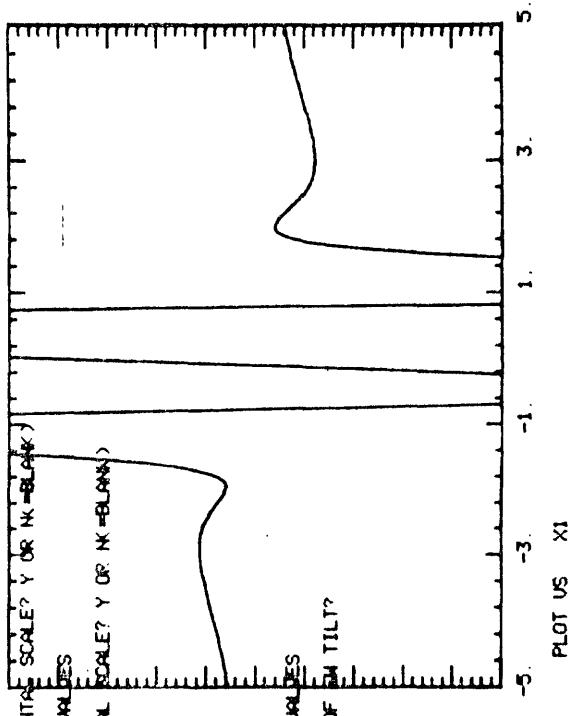
RCTNGL

Exponential Slip Distribution

Lines 57-59 have been changed to the exponential slip distribution indicated on the following page. Note that the tilt amplitude is not symmetric (page 1-37). The lack of symmetry is caused by the slip distribution specifying a larger displacement at the right-hand margin than at the left-hand margin of the slip zone.

1-31

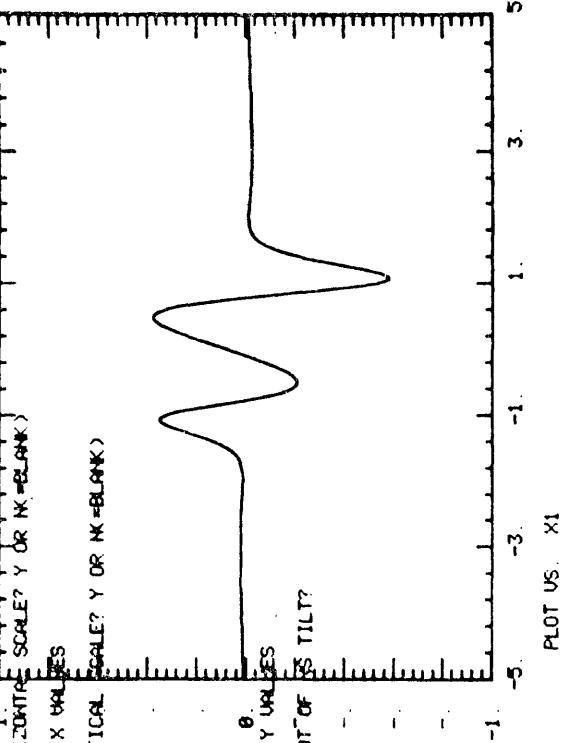
EXPONENTIAL SLIP DISTRIBUTION
 0=RE-START, 1=NEW PLOT
 1! SET HORIZONTAL SCALE? Y OR N=BLANK
 Y!
 MIN/MAX X VALUES
 -5.5!
 SET VERTICAL SCALE? Y OR N=BLANK
 E



PLOT US X1

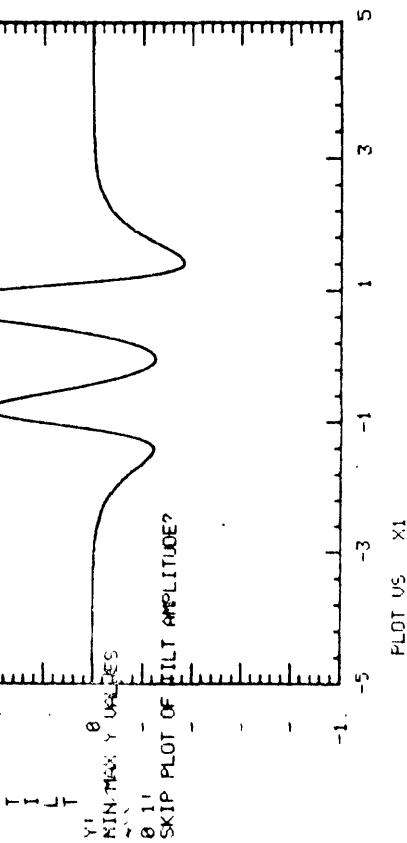
1-31

EXPONENTIAL SLIP DISTRIBUTION
 0=RE-START, 1=NEW PLOT
 2! SET HORIZONTAL SCALE? Y OR N=BLANK
 Y!
 MIN/MAX X VALUES
 -3.5!
 SET VERTICAL SCALE? Y OR N=BLANK
 E

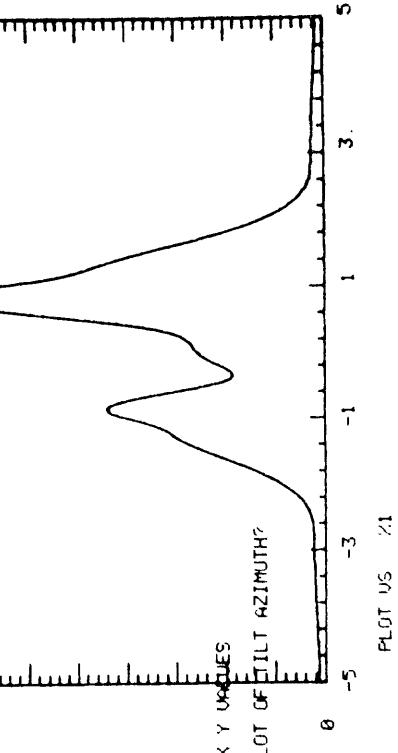


PLOT US X1

EXPONENTIAL SLIP DISTRIBUTION
 $\theta = RE-START, 1=NEW PLOT$
 $2=SET HORIZONTAL SCALE? Y OR N=BLANK,$
 $Y1=MIN-MAX X VALUES$
 $-5, 5$
 $S=SET VERTICAL SCALE? Y OR N=BLANK)$

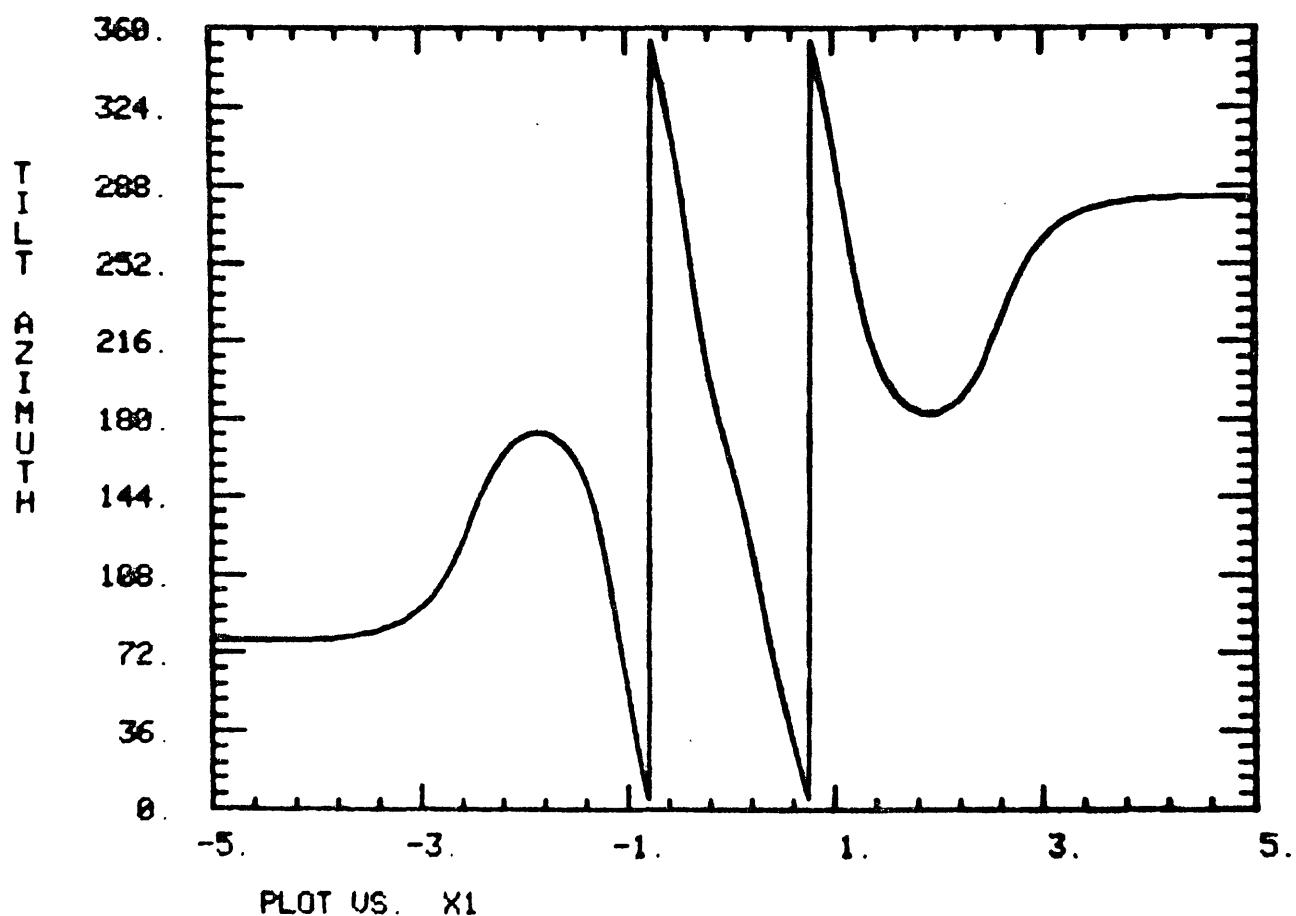


EXPONENTIAL SLIP DISTRIBUTION
 $\theta = RE-START, 1=NEW PLOT$
 $2=SET HORIZONTAL SCALE? Y OR N=BLANK,$
 $Y1=MIN-MAX X VALUES$
 $-5, 5$
 $S=SET VERTICAL SCALE? Y OR N=BLANK)$



1-38

EXPONENTIAL SLIP DISTRIBUTION



DOCUMENTATION OF RCTNGL

18 JUN 70 09.44.15 MCNAUGH .RCTNGL

```

1  DELETE(LGU,LUTPUT,RCTNGL)
2  RCTNGL.
3  CXIT.
4  LIUCOPY(GRAPHIC,TXLG0/RR,TXLGC)
5  LIUCOPY(JURAT,NPLGU/RK,NPLGC)
6  DELETE(LGG,LUTPUT,RCTNGL)
7  KUNZE()
8  LINK(F=LGG,F=TXLGC,F=NPLGC,B=RCTNGL)
9  RCTNGL.
10 FILE.
11 EOF
12      E:CGRAM FLTNGL(TAPEPTY=201,FILM=TAPEPTY,TAPE 7=TAPEPTY)
13  COMMON/TVPOL/TVPOL(3)
14  COMMON/TVTUNE/VTUNE(30)
15  COMMON/JPLCT/XLT,XRT,YLC,YLP,MAJX,MAJY,KX(2),KY(2),
16  LTITLE(3),LU,LTF,LNLGX,LNLGY,NCLX,NCLY,LTITLE(8)
17  DIMENSION IFET(3)
18  DIMENSION AX1(200),AX2(200),THETA1(20,20),THETA2(20,20)
19  DIMENSION TNU(200),TLW(200),TAUH(200),TAZM(200),T(200),AB(20)
20  CALL FLT(5LTAP7,IFET,0)
21  IFET(2)=IFET(2).OR.LU000 0010 0000 0000 000008
22  IFET(3)=IFET(3).OR.46000 0000 0000 0000 000008
23  CALL FLT(5LTAP7,IFET,-8)
24  113 CONTINUE
25  HAA=1.234E-20 BWRITE(7,3)
26  3 FORMAT(*1=PLOT VS. X1, 2=PLOT VS. X2*)
27  CALL GLTRUM(AB) BIFLAG=AB(1) BWRITE(7,3)
28  9 FORMAT(*SPECIFY INITIAL AND FINAL POINTS OF PLOT*)
29  CALL GLTRUM(AB) B1=0.0=A3(1) BEND=A3(2)
30  IF(IFLAG.EQ.1)KHOLD=2HX2 BIFLAG=IFLAG.EQ.2)KHOLD=2HX1
31  WRITE(7,1)KFIELD &CALL GLTRUM(AB) CONSTNT=AB(1)
32  10 FORMAT(*SPECIFY VALUE OF *,AB,* THAT PROFILE IS COMPUTED FOR*)
33  WRITE(7,11)
34  11 FORMAT(*SPECIFY C1X1FN,C1X3FN,C2X3FN,C3X1FN*)
35  CALL GLTRUM(AB) BC1X1FN=AB(1) BC1X3FN=AB(2) BC2X3FN=AB(3)
36  BC3X1FN=AB(4) BNFT..(7,12)
37  12 FORMAT(*SPECIFY NUMBER OF POINTS IN PROFILE,*,*,
38  1           *NUMBER OF COLUMNS AND ROWS,*,*,
39  1           *SPATIAL FREQUENCY OF SLIP IN X1 DIRECTION,*,*,
40  1           *SPATIAL FREQUENCY OF SLIP IN X3 DIRECTION,*,*,
41  1           *A1 MAXIMUM SLIP*)
42  CALL GLTRUM(AB) BM=AB(1) BN1=AB(2) BN2=AB(3) BFREQX1=AB(4)
43  FN1X3=AB(5) BMAX=AB(6) BWRITE(7,13)
44  13 FORMAT(*SPECIFY ANGLE OF FAULT TO NS AXIS, IN DEGREES*)
45  CALL GLTRUM(AB) BTHETA=AB(1) BAL=C1X1FN-C3X1FN
46  W=C2X3FN-C1X3FN BCT=COS(THETA*.01745) BST=SIN(THETA*.01745)
47  DO 1 K=1,M
48  YINC=(INU-BEGIN)/M
49  IF(IFLAG.EQ.1)AX1(K)=BEGIN+(XINC*(K-1))
50  IF(IFLAG.EQ.1)AX2(K)=CONSTNT
51  IF(IFLAG.EQ.2)AX1(K)=CONSTNT
52  IF(IFLAG.EQ.2)AX2(K)=BEGIN+(XINC*(K-1))
53  DO 2 I=1,N
54  DO 3 J=1,N
55  C1X1=C3X1FN+((AL/N1)*J) BC1X3=C1X3FN+((W/N2)*(I-1))
56  C2X3=C1X3+(W/N2) BC3X1=C1X1-(AL/N1)
57  U=-U1AX*COS(((U1X1-C3X1FN)/AL)*2.*3.14159*FREQX1)*
58  1  BC3(((C2X3-U1X3FN)/W)*2.*3.14159*FREQX3)

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59      U=-ABS(U)
60      X1=AX1(K)  BX2=AX2(K)
61      CALL CMPTLT(U,X1,X2,C1X1,C1X3,C2X3,C3X1,A,B)
62      THETA1(I,J)=A
63      S THETA2(I,J)=B
64      C CONTINUE
65      SUM1=SUM2=0.
66      DO 4 I=1,N2
67      DO 5 J=1,N1
68      TNU(K)=THETA1(I,J)+SUM1
69      TKE(K)=THETA2(I,J)+SUM2
70      SUM1=TNU(K)
71      SUM2=TKE(K)
72      C CONTINUE
73      A=TNs(K)  BB=TEW(K)
74      TKE(K)=A*TU+B*BT
75      TEW(K)=-A*TU+B*BT
76      TAMPM(K)=SIGN((TKE(K)**2)+(TNs(K)**2))
77      IF(TNs(K).EQ.0.) TNU(K)=1.E-20
78      TA21(K)=(ATAN(TKE(K)/TNs(K)))*(180./3.1415926)
79      IF(TNs(K).LT.0.) TAZM(K)=TAZM(K)+180.
80      IF(TAZM(K).LT.0.) TAZM(K)=TAZM(K)+360.
81      IF(TAZM(K).GT.360.) TAZM(K)=TAZM(K)-360.
82      DO 7 I=1,N1
83      IF(IFLAG.EQ.1) AX1(I)=AX1(J)
84      IF(IFLAG.EQ.2) T(I)=AX2(I)
85      TNsMIN=TNs(1)  STNSMIN=TNs(1)  BTAMPMD=TAMP(1)  STAZMMD=TAZM(1)
86      TEWMIN=TEW(1)  BTENMAX=TEW(1)  BTNSMIN=TNs(1)  BTNSMAX=TNs(1)
87      TAMPMN=TAMP(1)  BTAZMMN=TAZM(1)  BTAZMMX=TAZM(1)
88      DO 150 I=1,N1
89      IF(TEW(I).LT.TEWMIN) TEWMIN=TEW(I)
90      IF(TEW(I).GT.TEWMAX) TEWMAX=TEW(I)
91      IF(TNs(I).LT.TNSMIN) TNSMIN=TNs(I)
92      IF(TNs(I).GT.TNSMAX) TNSMAX=TNs(I)
93      IF(TAMP(I).LT.TAMPMN) TAMPMN=TAMP(I)
94      IF(TAMP(I).GT.TAMPMX) TAMPMX=TAMP(I)
95      IF(TAZ(I).LT.TAZMMN) TAZMMN=TAZM(I)
96      IF(TAZ(I).GT.TAZMMX) TAZMMX=TAZM(I)
97      150 CONTINUE
98      WRIT(7,17) TEWMIN,TEWMAX,TNSMIN,TNSMAX,TAMPMN,TAMPMX,TAZMMN,TAZMMX
99      17 FORMAT(*MIN./MAX. VALUES OF EW COMPONENT*,2X,E10.3,2X,E10.3,/,1
100      1 *MIN./MAX. VALUES OF NS COMPONENT*,2X,E10.3,2X,E10.3,/,1
101      1 *MIN./MAX. VALUES OF AMPLITUDE*,5X,E10.3,2X,E10.3,/,1
102      1 *MIN./MAX. VALUES OF AZIMUTH*,3X,F10.3,2X,F10.3,/,1
103      1 *(NOT TILT AMPLITUDES ARE IN MICRORADIAN*,/,1
104      1 *AZIMUTH IN DEGREES*)*
105      170 WRIT(7,170)
106      170 FORMAT(*THE FOLLOWING ARE PLOTS OF THE EW AND NS *,/,1
107      1 *COMPONENTS OF TILT, AND THE TILT AMPLITUDE*,/,1
108      1 *AND AZIMUTH (MEASURED CLOCKWISE FROM NORTH)*,/,1
109      1 *ENTER STATE, 1=CONTINUE*)*
110      CALL OUTNUM(AB)  B1<FLAG=AB(1)
111      IF(1<FLAG.EQ.1) GO TO 113
112      LBL=7  BNLU=X=1  BNLYU=1  BNLYX=2  BNLY=2
113      BNLY(7,1)=0
114      179 FORMAT(*TILT PLOT TITLE, 30 CHARACTERS*)
115      RLAD(7,2)=LTITLE(JM),JM=1,5
116      180 FORMAT(BA16)

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117 IF(LIFLAG.EQ.1)KX(2)=10HX1
118 IF(LIFLAG.EQ.2)KX(2)=10HX2
119 KX(1)=10H PLOT VS.
120 KF(1)=10H EW TILT
121 KY(2)=10H BMAJX=5 BMAYY=10 BLTITL? (1)=1
122 YUD XLT=T(1) BXRT=T(M) BYLC=TEWMIN BYUP=TEWMAX
123 WLT(7,70)
124 7U FFORMAT(*BLT HORIZONTAL SCALE? Y OR N(=BLANK)*)
125 FUD(7,66)CHARAC BIF(CHARAC.EQ.1HN.OR.CHARAC.EQ.1H)GO TO 71
126 WRITE(7,72)
127 72 FFORMAT(*MIN/MAX X VALUES*)
128 CALL GETNUM(AB) BXLT=AB(1) BXRT=AB(2)
129 71 WLT(7,73)
130 73 FFORMAT(*BLT VERTICAL SCALE? Y OR N(=BLANK)*)
131 FUD(7,66)CHARAC BIF(CHARAC.EQ.1HN.OR.CHARAC.EQ.1H)GO TO 74
132 WRITE(7,75)
133 75 FFORMAT(*MIN/MAX Y VALUES*)
134 CALL GETNUM(AB) BYLU=AB(1) BYUP=AB(2)
135 7+ IF(TEWMIN.LT.TEWMAX)YLU=YUP+1.
136 IF(TEWMAX.LT.TEWMIN)YUP=YUP+1.
137 WRITE(7,109)
138 109 FFORMAT(*SKIP PLOT OF EW TILT?*)
139 :EAD(7,66)IJVAR
140 UC FFORMAT(AI)
141 LF(IJVAR,LG.1HN.JR.,IJVAR.EQ.1H)CALL PLOTS(TEW,T,1,M)
142 WLT(7,76)SCALE GETNUM(AB)BIKFLAG=AB(1)
143 If(IKFLAG.EQ.0)GOT0113BIF(IKFLAG.EQ.1)GOT0903
144 YU(1)=10H NS TILT BXLT=T(1) BXRT=T(M)
145 KY(2)=10H
146 YLU=TNSMIN BYUP=TNSMAX BWRITE(7,76)BREAD(7,66)CHARAC
147 LF(CHARAC.EQ.1HN.OR.CHARAC.EQ.1H)GOT0710
148 WLT(7,77)ECAU GETNUM(AB)BXLT=AB(1)BXRT=AB(2)
149 WLT(7,78)ECAU(7,78)CHARAC
150 LF(CHARAC.EQ.1HN.OR.CHARAC.EQ.1H)GOT0740
151 WLT(7,79)ECAU GETNUM(AB)BYLO=AB(1)BYUP=AB(2)
152 If(YLU.EQ.YUP)AAA=YLU$BIF(YLU.EQ.AAA)YUP=YUP+1.
153 If(YLU.EQ.AAA)YLO=YLO-1.
154 WRITE(7,710)BREAD(7,66)IJVAR
155 910 FFORMAT(*SKIP PLOT OF NS TILT?*)
156 If(IJVAR,LG.1HN.OR.,IJVAR.EQ.1H)CALL PLOTS(TNS,T,1,M)
157 WRITE(7,711)
158 118 FFORMAT(*L=AM=START, 1=NEW PLOT*)
159 CALL GETNUM(AB)BIKFLAG=AB(1)
160 If(IKFLAG.EQ.1)GU IC 113 BIF(IKFLAG.EQ.1)GOT0900
161 KY(1)=10H TILT AM=LI BXLT=T(1) BXRT=T(M)
162 KY(2)=10H TILT
163 YLU=TAMPMX BYUP=TAMPMX BWRITE(7,76)BREAD(7,66)CHARAC
164 LF(CHARAC.EQ.1HN.OR.CHARAC.EQ.1H)GOT0741
165 WLT(7,76)ECAU GETNUM(AB)BXLT=AB(1)BXRT=AB(2)
166 WLT(7,77)ECAU(7,77)CHARAC
167 LF(CHARAC.EQ.1HN.OR.CHARAC.EQ.1H)GOT0742
168 WLT(7,78)ECAU GETNUM(AB)BYLO=AB(1)BYUP=AB(2)
169 7+2 If(YLU.EQ.YUP)AAA=YLU$BIF(YLU.EQ.AAA)YUP=YUP+1.
170 If(YLU.EQ.AAA)YLO=YLO-1.
171 WRITE(7,712)BREAD(7,66)IJVAR
172 912 FFORMAT(*SKIP PLOT OF TILT AMPLITUDE?*)
173 If(IJVAR,LG.1HN.OR.IJVAR.EQ.1H)CALL PLOTS(TAMP,T,1,M)
174 WRITE(7,79)ECAU GETNUM(AB)BIKFLAG=AB(1)

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175      IF (IKFLAG.EQ.0) GOTO 01136 IF (IKFLAG.EQ.1) GOTO 0911
176 910 KY(1)=10HTILT AZIMU $XLT=T(1)$XRT=T(M)
177      KY(2)=10HTH      $YLC=TAZMMN $YUP=TAZMMX
178      WRITE(7,70) READ(7,60) CHARAC
179      IF (CHARAC.EQ.1HN.OR.CHARAC.EQ.1H) GOTO 0743
180      WRITE(7,72) &CALL GETNUM(AB) $XLT=AB(1)$XRT=AB(2)
181 743 WRITL(7,73) $- LAD(7,60)CHARAC
182      IF (CHARAC.EQ.1HN.OR.CHARAC.EQ.1H) GOTO 0744
183      WRITL(7,75) &CALL GETNUM(AB) $YLU=AB(1)$YUP=AB(2)
184 744 IF (YLU.EQ.YUP) AAA=YLC&IF (YLU.EQ.AAA) YUP=YUP+1.
185      IF (YLU.EQ.AAA) YLC=YLU-1.
186      WRITL(7,914) BACAU(7,60)IJVAR
187 914 FORMAT(*E8.8 IF PLOT OF TILT AZIMUTH?*)
188      IF (IJVAR.EQ.1HN.OR.IJVAR.EQ.1H) CALL PLOTS(TAZM,T,1,M)
189      WRITE(7,10) &CALL GETNUM(AB) &IF (AB(1).EQ.0.) GOTO 0113
190      STOP &EN
191      SUBROUTINE CMPTLT(U,X1,X2,C1X1,C1X3,C2X3,C3X1,T1,T2)
192      A1=A2=A3=A4=&U1=&U2=&U3=&U4=0.
193      X3=J. X2X1=C1X1+C3X3-C2X3&C4X1=C3X1&C4X3=C1X3
194      C1L= TILT(U,X1,X2,X3,C1X1,C1X3,A1,&U1)
195      C2L= TILT(U,X1,X2,X3,C1X1,C2X3,A2,&U2)
196      C3L= TILT(U,X1,X2,X3,C3X1,C3X3,A3,&U3)
197      C4L= TILT(U,X1,X2,X3,C4X1,C4X3,A4,&U4)
198      T1=A1+A2+A3+A4
199      T2= 1-B2+B2+B4
200      RETURN
201      END
202      SUBROUTINE TILT(X1,X1,X2,X3,P1,P3,T1,T2)
203      R=SQR((X1-P1)**2+X2**2+(X3-P3)**2)
204      R=R+P3
205      T1=(J1/J2.&R**4)*(X2*(X1-P1)*(R*R-(R+2.*P3)*(2.*R+P3)))/
206      1 (-**3*(P**2))
207      T2=(J1/J2.&R**4)*(X2**2*(R*R-(R+2.*P3)*(2.*R+P3))/(R**3*R**2)
208      1 +(R+2.*P3)/(R*R))
209      R=1U-N
210      ENL
211      SUBROUTINE GETNUM(N)
212      DIMENSION N(1),L(BU)
213      FLAD(7,3) L & J=U
214      U=U+1 & N=0=S=J & M=f=1
215      I=I+1 & IF (I.GT.BU) THEN TURN & J=L(I) & K=4
216      IF (L.GT.BU) K=2 & IF (L.GT.27.A.0.L.GT.30) K=1
217      IF (L.GT.47) K=3 & K=K+S & GOTO (1,2,3,5,1,4,3,4) K
218      1 N=N+16+U-27          S=4          S GOTO 5
219      2 M=-1                  S=4          S GOTO 5
220      3 P=1                  S=4          S GOTO 5
221      4 IF (P.LT.0) F=10.** (I-F-1) & F(J)=N/F*M & GOTO 6
222      5 F=F+141(BU-1)
223      ENL

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PROGRAM SLPPRP

PART 2

DOCUMENTATION FOR PROGRAM SLPPRP

INTRODUCTION:

Creep-related tilt changes can be approximated by modeling the slip distribution on the fault plane as an expanding dislocation loop with spatially and temporally varying displacement as discussed in McHugh and Johnston (1976) and McHugh (1976). The program and model in this section (which will be referred to as Model II) is an extension of the programs XPND/XPND01/XPND02 (which will be referred to as Model I) discussed in McHugh (1976).

Model I reproduces the creep-related tilt changes by computing the quasi-static tilts, at the free surface of an elastic medium, associated with a vertically oriented rectangular dislocation loop (Press, 1965). The slip distribution is constant, at any given instant, across the slip surface; but varies in time. This particular approximation however does not reproduce the entire slip distribution as a function of time as shown in figure 2.1. Notice that when the slip surface encompasses rectangle HIJD the displacement versus time profile seen by a creepmeter is a single point.

Model II (figure 2.2) uses a somewhat more realistic approximation to reproduce the creep-related tilts. In this model, the entire slip versus time function is computed for each rectangle as the dislocation loop expands. With this procedure the effect of the propagating boundary is somewhat independent of the effect of the slip as a function of time at points within the slip zone. Because the medium is elastic the rule of superposition can be used to express the tilt at a point on

the free surface. If θ is the tilt component, i is the time after the start of the slip zone expansion, and j is the time after initiation of slip at a point m, the tilt versus time profiles will appear as in figure 2.3. The tilt, T_k , (either $\frac{\partial w}{\partial x}$ or $\frac{\partial w}{\partial y}$ at a time k after the start of the zone expansion) is given by

$$T_k = \sum_{j=1}^k \theta_{j, k-j+1} - \sum_{j=1}^{j=k-1} \theta_{j, k-j} .$$

For example, the tilt at $t=3$ units after the zone starts to expand (figure 2.3) is:

$$\begin{aligned} T_3 &= \theta_{1,3} + (\theta_{2,2} - \theta_{1,2}) + (\theta_{3,1} - \theta_{2,1}) \\ &= (\theta_{1,3} + \theta_{2,2} + \theta_{3,1}) - (\theta_{2,1} + \theta_{1,2}) . \end{aligned}$$

INPUT:

The working arrays, examples of various slip distributions, and notation used are given in McHugh (1976). The expressions used to compute the tilts are given in Press (1965). Unlike Model I, the slip zone expansion velocity need not be constant but can be exponential or some combination of exponential and constant velocities. The positions of the boundaries of the slip zones (strike-slip or dip-slip) can be incremented exponentially (eg. curve P Q R, figure 2.2) and/or linearly (eg. curve TUV, figure 2.2). The slip-time function may be linear or exponential (profiles PP' through VV' - figure 2.2), and will be the same for each slip rectangle (eg. rectangles ABCD, EFGD, and HIJD - figure 2.2). Notice too that curve PQR (figure 2.2) physically corresponds to

creep onset-times that decay exponentially, while curve TUV produces a linear creep onset-time distribution. To produce a reference line on the tilt-time displays, the slip zone is fixed at its initial position for the first N units after the start of the computations and fixed in its final position for the last 'NRECPT-N3' units (figure 2.4). The tilts produced by a strike-slip zone and a dip-slip zone may be combined as discussed in McHugh (1976) for Model I. Provision is also made in Model II for one zone to trigger the other's growth.

Model II is intended for use at the Tektronix 4010-1 terminal and is stored at LBL. Once the user is logged onto the 6600 B or C machine with 100 K of core, Model II may be accessed using:

^LOAD, SLPPRP, MCHUGH

The program links automatically to the necessary plotting routines so that the ^LOAD command may be followed immediately by:

^RUN

Examples of the program in operation are given on pages 2-19 to 2-59.

The following is a step-by-step list of the input the computer requires.

1) 1 = Zone Expands, 2 = Zone Contracts

Entering a 1 causes the zone to grow from its initial to its final values; a 2 causes the reverse to occur (ie. the zone appears to 'collapse').

2) 1/2 = Slip incremented exponentially/linearly

Strike-Slip/Dip-Slip

Enter 2 numbers (eg. 1 (space) 1). The first number causes the displacement on the strike-slip zone to be incremented linearly (2) or exponentially (1), while the second number controls the slip-time function on the dip-slip zone.

3) 0 = Increment corners separately

1/2 = Increment all corners exponentially/linearly

Strike - slip/Dip-slip

Enter 2 numbers (eg. 1 (space) 0). The corners of the strike-slip zone (controlled by the first number) and dip-slip zone (second number) will be incremented exponentially (1) or linearly (2); or the corners may be controlled individually by entering a zero. If both numbers are a 1 or a 2, the program skips to part 4 below. If a zero is entered the computer responds:

a) 1 = Variable incremented exponentially

2 = Variable incremented linearly

b) activated if the second number is zero

D1X1, D1X3, D2X3, D3X1

Enter 4 numbers.

c) activated if the first number is zero

C1X1, C1X3, C2X3, C3X1

Enter 4 numbers.

4) 'U1>0' = left-lateral strike-slip

'U3>0' = 'X2>0' side down

U1IN, U1FN, U3IN, U3FN

Enter 4 numbers for the initial (IN) and final (FN) slip values. The slip will be incremented between its initial and final values in a linear or exponential fashion depending upon which options were selected in part 2 above.

5) 'TRIGGER' option desired?

Enter a yes (Y) or no (N). This option is the same as discussed in programs XPND/XPND01/XPND02 (McHugh, 1976). If N is entered, the

program moves to part 6 below.

a) $0 = D(I1) > C(I2)$, $1 = D(I1) < C(I2)$

The '0' option is equivalent to the trigger option in programs XPND/XPND01, the '1' option to program XPND02 (McHugh, 1976). When the corner designated by $D(I1)$ is greater than (0) or less than (1) the corner designated by $C(I2)$, the appropriate zone is triggered (ie. starts 'growing').

b) $0 = \text{Strike-slip}/l = \text{Dip-slip zone triggered}$

Entering a zero causes the dip slip zone to trigger the strike-slip zone; a 1 causes the strike-slip zone to trigger the dip-slip zone.

c) Specify I1 and I2

Enter 2 numbers corresponding to numbers of the C and D arrays as shown in part 5a above. The C and D arrays are given in McHugh (1976).

6)

a) activated if $U1IN$ and $U1FN$ in part 4 are both non-zero

$C1X1IN, C1X3IN, C2X3IN, C3X1IN, C1X1FN, C1X3FN, C2X3FN, C3X1FN$

Enter the 8 coordinates required for the strike-slip zone.

b) activated if $U3IN$ and $U3FN$ in part 4 are both non-zero.

$D1X1IN, D1X3IN, D2X3IN, D3X1IN, D1X1FN, D1X3FN, D2X3FN, D3X1FN$

Enter the 8 coordinates required for the dip-slip zone.

7) Enter station coordinates - ($X1, X2$)

Enter the $X1$ and $X2$ coordinates of the station.

8) Specify 2 corners of dislocation surface for display

$1 = D1X1 = D2X1$

$2 = D1X3 = D4X3$

$4 = D2X3 = D3X3$

$5 = D3X1 = D4X1$

$9 = C1X1 = C2X1$

$10 = C1X3 = C4X3$

$12 = C2X3 = C3X3$

$13 = C3X1 = C4X1$

Enter 2 numbers to display the position of the desired corners as a function of time.

9) To display slip as a function of time

Enter zone index, Caution -

Index must be between 1 and (INDEX)

(INDEX) is the total number of slip rectangles used in the computation.

Enter the number corresponding to the slip zone desired. This number will cause the slip as a function of time for that slip zone to be displayed in the output.

10) Theta = angle between strike of fault

And north = (NUMBER) Degrees

No response required. The value of theta is printed.

11) MIN/MAX values of EW component (numerical values)

MIN/MAX values of NS component (" ")

MIN/MAX values of amplitude (" ")

MIN/MAX values of azimuth (" ")

(Note: Tilt amplitudes are in microradians, azimuth in degrees)

The following are plots of the EW and NS components of tilt, and the tilt amplitude and azimuth (measured clockwise from north).

0 = Re-start, 1 = Continue

Enter a zero or one as desired. A zero will cause all the output to be skipped and the program to be re-started. The following occur if a 1 is entered.

12) Write plot title, 80 characters

Enter up to 80 alphanumeric characters.

13) The procedure for scaling the graphs in the output are the same as discussed in McHugh (1976) and will not be discussed here.

14) The graphs are displayed automatically once the scaling and 'skip' options are selected.

OUTPUT:

The plots occur in the following order:

- 1) EW tilt component versus time
- 2) NS tilt component versus time
- 3) Theta 2 versus time
- 4) Theta 1 versus time
- 5) Strike-slip versus time
- 6) Dip-slip versus time
- 7) Tilt amplitude versus time
- 8) Tilt azimuth versus time
- 9) Corner 1 versus time
- 10) Corner 2 versus time
- 11) Strike-slip area versus time
- 12) Dip-slip area versus time

'Time' in parts 1, 2 and 7 through 12 is the time after the start of the slip zone expansion, and corresponds to the individual rectangles for which the tilts, $\theta_{i,j}^m$, are computed, 'Time' in parts 3 through 6 is the time after the start of slip on the individual slip zone. Theta 1 and Theta 2 are $\frac{\partial w}{\partial x_1}$ and $\frac{\partial w}{\partial x_2}$ in Press' (1965) notation and correspond to $\theta_{i,j}^m$ in figure 2.3. Corners 1 and 2 correspond to the corners selected in part 8 of the Input section.

After the dip-slip area has been displayed, or if the '0 = Re-start' option is selected, the C array is printed out as follows:

C(1)	C(2) . . .	C(6)
:		:
C(30)	. . .	C(36)

The C array contains the initial and final values of the coordinates and slip (McHugh, 1976). This array is followed by:

ICRNR(1)		ICRNR(8)		
:		:		
ICRNR(9)		ICRNR(16)		
IT(1) . . . IT(4)		ITIME		
KFLAGS	KFLAGD	LFLAG	MFLAG	IFLAG
NRECPT	N	N1	N2	N3

Definitions of these variables will be found in Appendix A (page 2- 11). A list of options for re-starting the program follows these variables:

- 1 = Re-start with all new values
- 2 = Re-start with new strike-slip value and zone coordinates
- 3 = Re-start with new dip-slip value and zone coordinates
- 4 = Re-start with new strike-slip value only
- 5 = Re-start with new dip-slip value only
- 6 = Re-start with new tiltmeter coordinates only
- 7 = Stop

Entering a 1 through 6 will re-start the program with the changes specified above. The computer will request the information it needs. A 7 causes the program to stop.

RESULTS AND DISCUSSION:

Examples of the program operation start on page 2-19, and the program listing starts on page 2- 60. Appendix A (page 2- 11) lists some of the flags and their definitions.

The tilts from Model II are nearly the same as those from Model I if

- 1) the slip is constant in time (ie. U1IN = UIFN and U3IN = U3FN) and
- 2) the corners of the slip zone are incremented linearly. If the slip is constant in time, but the corners are incremented exponentially, the tilt-time curve (from Model II) will be compressed in time accordingly. If the slip is not constant in time and the corners are incremented exponentially and/or linearly, the tilt-time curve (Model II) will be reduced in total amplitude and stretched or compressed compared to Model I. The reduction in amplitude occurs because the slip is no longer constant over the entire slip zone but rather varies from near-zero at the edges to its maximum in the center. When the rectangle (slip zone) has stopped expanding, the slip at its margins is still increasing to the final slip value; consequently the tilt approaches its final value more slowly than the corresponding case in Model I.

Discontinuities may appear if the 'trigger' parameters allow the triggered and triggering zones to be meshed improperly (eg. if the slip on the triggered zone increases from its initial to final value discontinuously). If the tilt-time curves are continuous, the discontinuity near the start of the tilt azimuth curve is produced by zeroes in the initial values of the north-south tilt component. This particular discontinuity is an artifact of the computational procedure and does not represent an actual discontinuity in the tilt field.

STRTCH

Program STRTCH is a variation of SLPPRP that computes the maximum tilt amplitude seen at a station (with coordinates X1, X2) as a function of depth to the lower edge of the slip zone. STRTCH requires 100k of core and is accessed by: ^LOAD, STRTCH, MCHUGH. The geometry and notation in, operation of, and input to STRTCH is the same as SLPPRP. The only new parameters are DEPTHL (the depth to the lower boundary of the slip zone) and DELTAX (the amount by which DEPTHL is incremented). The initial and final values of the lower boundary are fixed for each computation (ie. C(4) = C(6) = C(12) = C(14) = C(20) = C(22) = C(28) = C(30) = DEPTHL). Although the lower edge is fixed, the other boundaries are free; and the tilt components at the station are computed in the same fashion as in SLPPRP. The maximum amplitude of the waveform is computed for each value of DEPTHL. The output is a display of the maximum tilt amplitude in microradians versus depth to the lower boundary of the slip zone in kilometers (examples are provided on pages 2-70 to 2-92, the program listing starts on page 2-93).

Note: Although the program requires specification of C2X3 and D2X3, the position of the lower boundary is actually determined by DELTAX and the maximum value of KTEST (line 217). Further, the position of the lower boundaries of the strike-slip and dip-slip zones are set equal to one another (lines 79-80). Each cycle through the program requires approximately 160 c.u.'s.

APPENDIX A

Flags Used In SLPPRP

Iflag: determines whether zone expands or contracts

Kflags, Kflagd: determines whether strike-slip (kflags) and dip-slip (kflagd) are incremented linearly or exponentially as a function of time

Lflag: determines whether all the strike-slip zone boundaries are incremented linearly or exponentially or are controlled separately

Mflag: acts in the same fashion as Lflag, but is used to control the dip-slip zone expansion

IT(1): determines whether triggered zone starts expanding when D(IT(3)) > C(IT(4)) or when D(IT(3)) < C(IT(4))

IT(2): determines whether the strike-slip or the dip-slip zone is triggered

IT(3), IT(4): determines which coordinates cause triggering (see IT(1))

ITIME: time, after start of triggering zone's expansion, that triggered zone's expansion starts; if not used, ITIME will have a value of 99999.

ICRNR: controls growth of zone coordinates (exponential = 1, linear = 2), index of ICRNR corresponds to index of D array

NRECPY: number of subrectangles used in computations (corresponds to number of time points after computations begin)

NSLPPT: number of time points in slip versus time profile

N, N1, N2, N3: indices used internally to scale zone expansion (see figure 2.4)

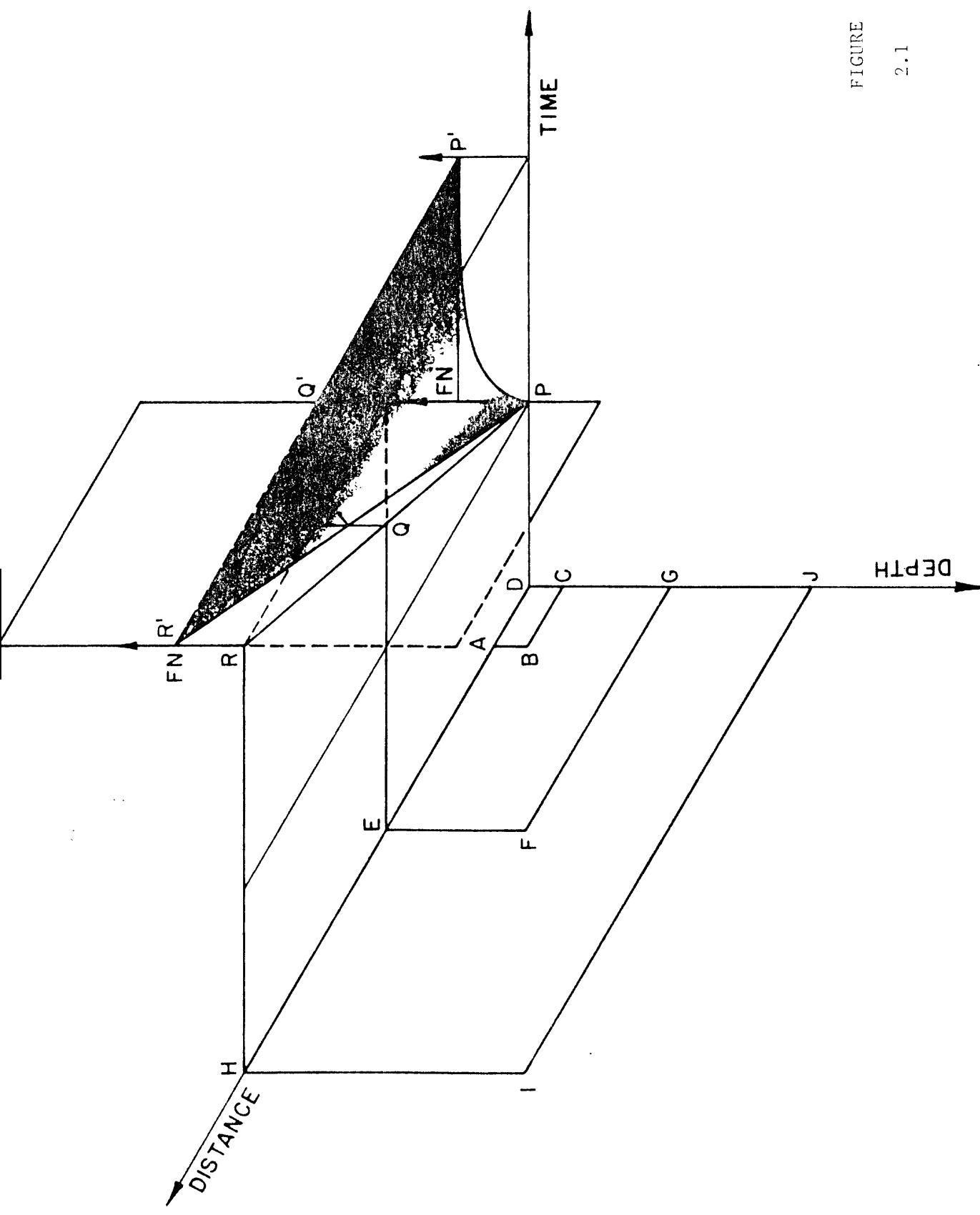
C and D arrays: defined in Appendix A of McHugh (1976); C is the array of initial and final values, D is the working array.

FIGURE CAPTIONS

- 2.1) Model I: Model of creep event used to predict tilt versus time profile. Dislocation loop expands from ABCD to HIJD. Corner A moves to position H linearly in time (indicated by line PQR). Only a point at position D 'sees' the entire slip versus time profile (PP'). Other points (eg. E and H) 'see' only a portion of the slip-time profile (QQ' and RR'). FN is the final slip value.
- 2.2) Model II: Model of creep event used to predict tilt versus time behavior. Dislocation loop expands in 'Distance-Depth' plane from ABCD to EFGD to HIJD. Curve PQR indicates that the position of the boundaries AB, EF, and HI vary exponentially in time (ie. the creep onset-times are distributed exponentially). Curve TUV indicates that the position of the lower boundary varies linearly with time. Curves PP' through VV' are the slip versus time profiles for the dislocation loop positions indicated. The slip as a function of position at a given instant can be determined by noting the slip, on profiles PP' through RR' or TT' through VV', along a constant-time line.
- 2.3) Model II: Tilts, $\theta_i^m{}_j$, generated by expansion of dislocation. Subscript 'i' denotes time after start of rupture, 'j' denotes time after start of slip at position 'm'. Time lines designated by ' T_i ' indicate tilts produced by spatially variable slip distribution; time lines designated by ' ΔT_i ' indicate tilts produced by temporally variable slip distribution.

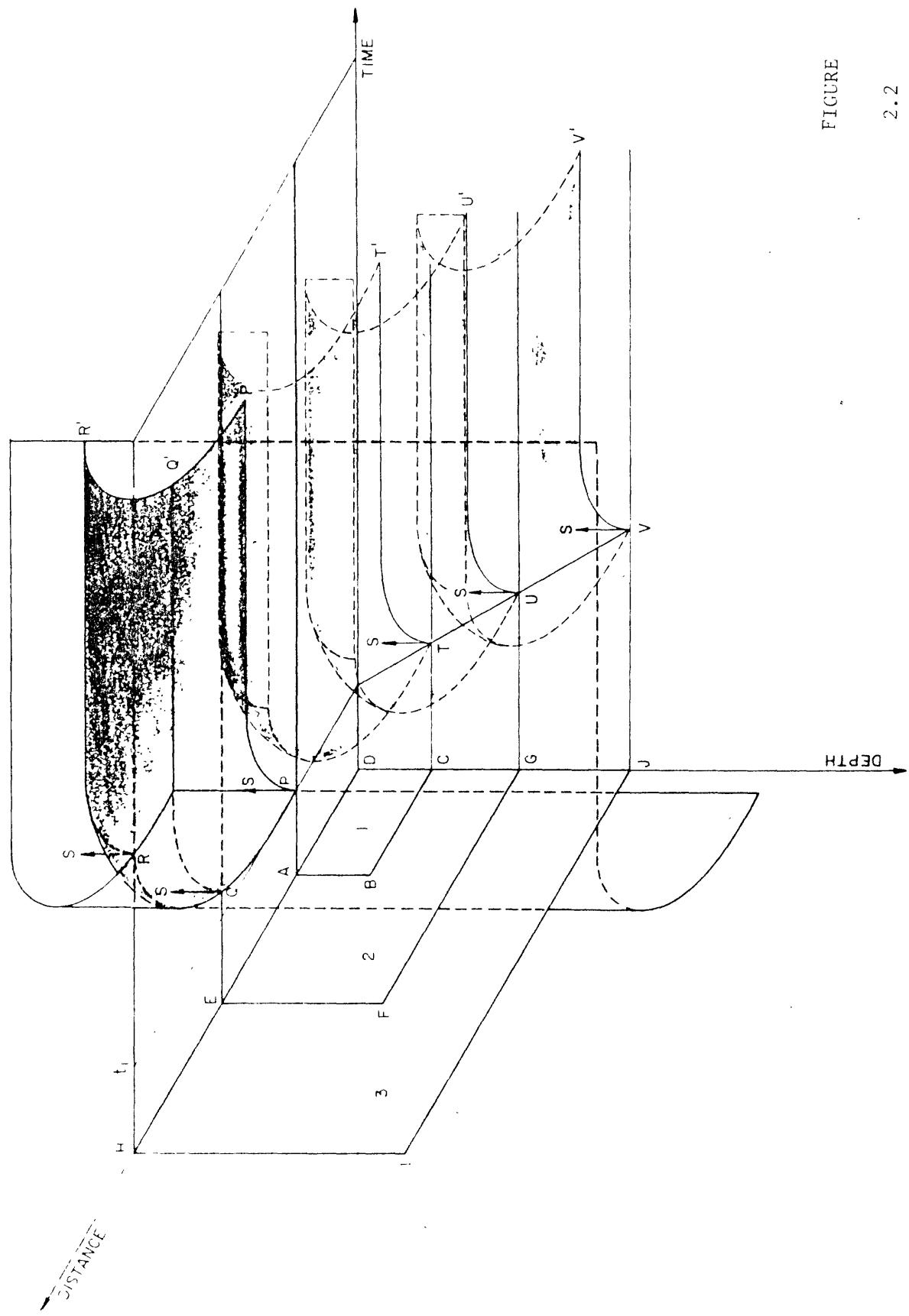
2.4) Model II: Slip versus time profiles used in program SLPPRP. The slip and zone coordinates are constant for the first N units after the computations begin. The slip zone coordinates are fixed at their final positions for computations steps N3 through NRECPT.

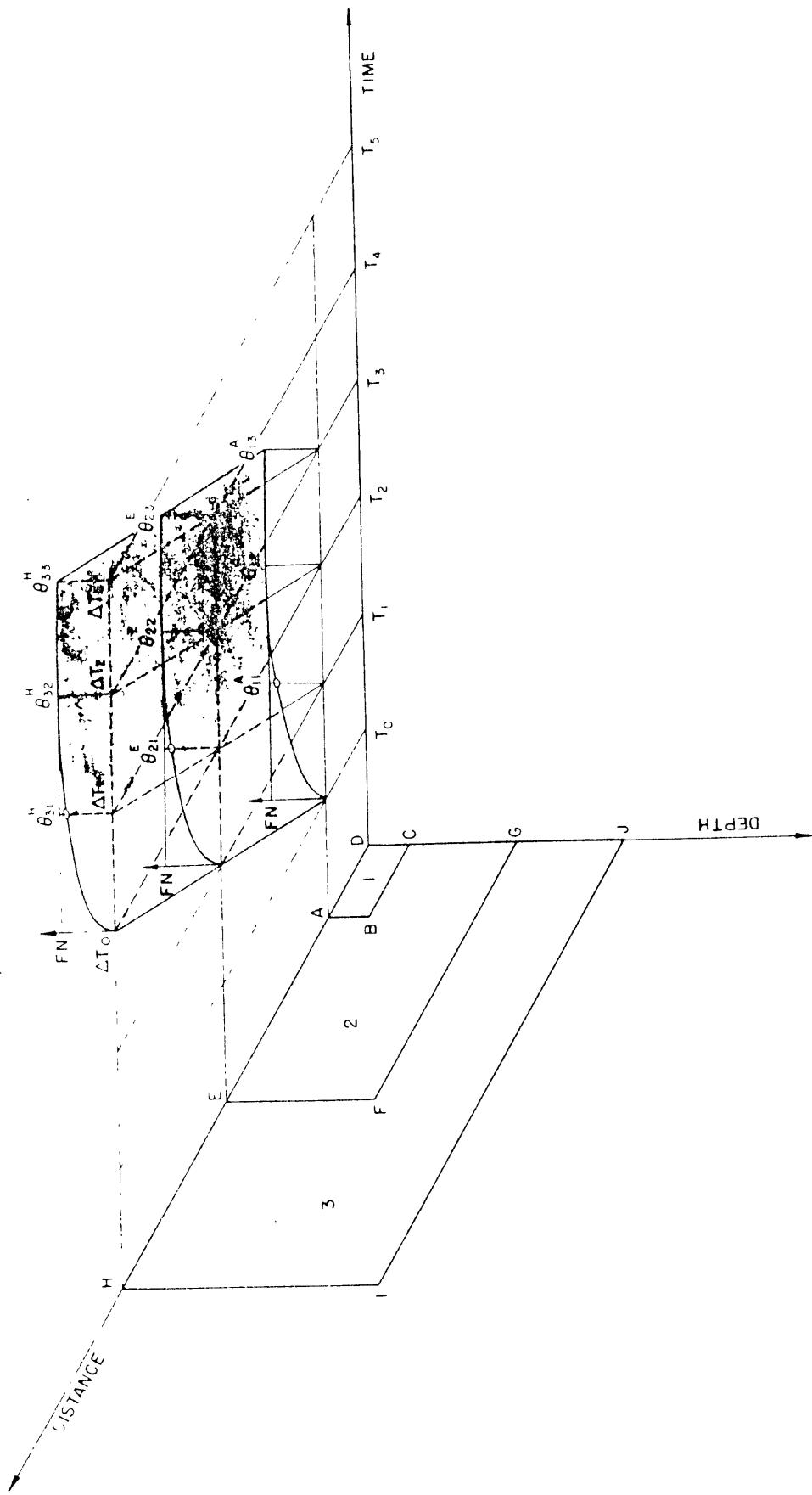
FIGURE
2.1



FIGURE

2.2

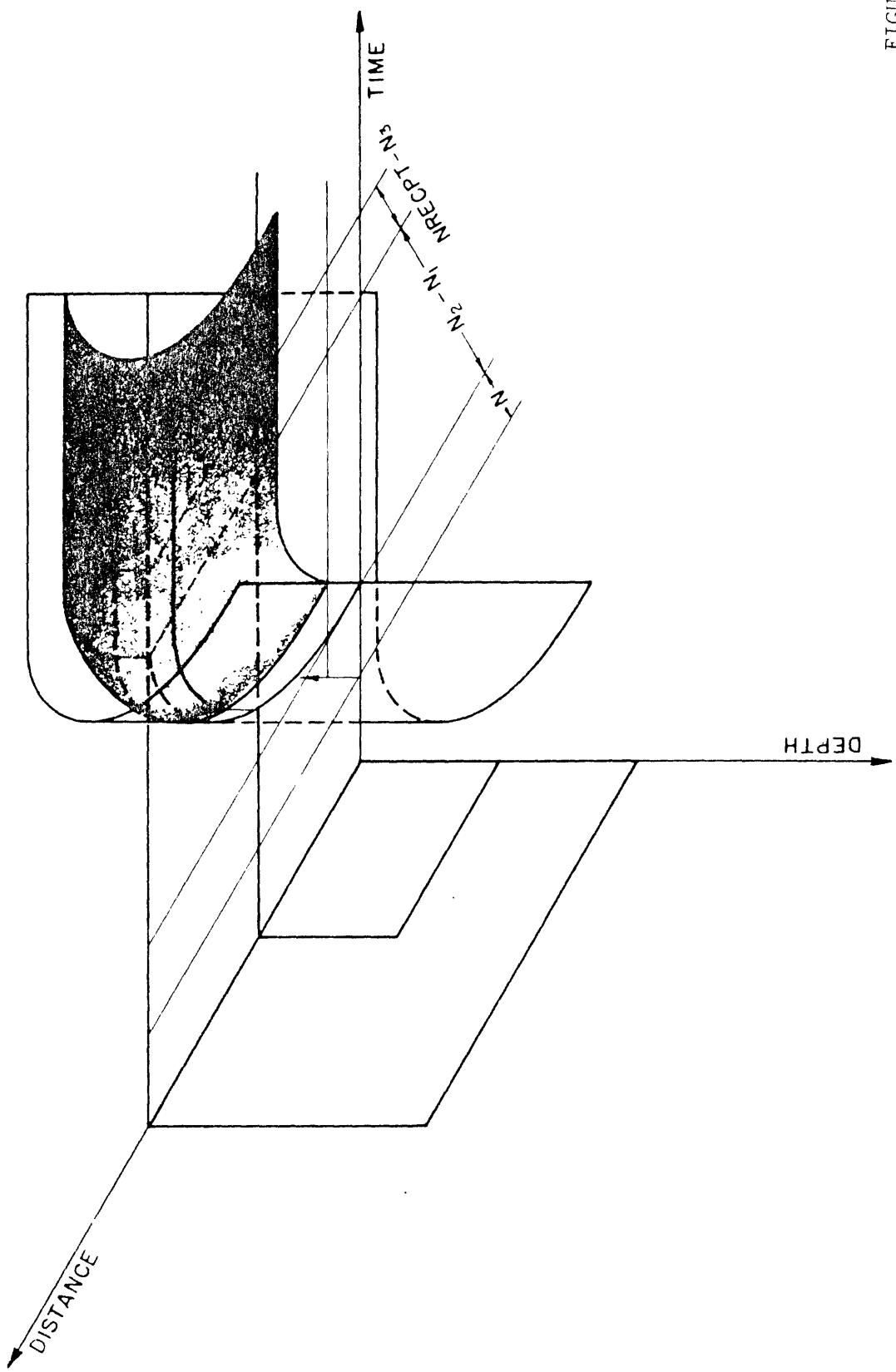




FIGURE

23

FIGURE



REFERENCES

McHugh, Stuart and Malcolm J. S. Johnston. Some short period nonseismic tilt perturbations and their relation to episodic slip on the San Andreas fault in central California, *J.G.R.*, in press, 1976.

McHugh, Stuart. Documentation of programs that compute 1) quasi-static tilts produced by an expanding dislocation loop in an elastic and viscoelastic material, and 2) surface shear stresses, strains and shear displacements produced by screw dislocations in a vertical slab with modulus contrast, U.S. Geol. Survey Open-File Report, 76-484

Press, Frank, Displacements, strains, and tilts at teleseismic distances, J.G.R., 70, 2395-2412, 1965.

EXAMPLES OF SLPPRP

THE TH-ANGLE BETWEEN STRIKE OF FAULT
 AND NORTH = 45.000 DEGREES
 MIN MAX VALUES OF EW COMPONENT -1 4.93E-01
 MIN MAX VALUES OF NS COMPONENT -1 2.92E-01
 MIN MAX VALUES OF AMPLITUDE 0 1.783E-01
 MIN MAX VALUES OF AZIMUTH 0 315.000
 (NOTE--TILT AMPLITUDES ARE IN MICRORADIAN,
 ACIMUTH IN DEGREES)
 THE FOLLOWING ARE PLOTS OF THE EW AND NS COMPONENTS
 OF TILT, AND THE TILT AMPLITUDE
 AND AZIMUTH (MEASURE CLOCKWISE FROM NORTH).
 PRE-START 1=CONTINUE
 11 WRITE FILE TITLE, 80 CHARACTERS
 LATERAL AND VERTICAL MIGRATION CONSTANT SLIP!
 SET HORIZONTAL SCALE? Y OR N (=BLANK)
 SET VERTICAL SCALE? Y OR N (=BLANK)
 Y!
 MIN MAX Y VALUES
 -5 5!
 SKIP PLOT OF EW TILT?

LATERAL AND VERTICAL MIGRATION-CONSTANT SLIP

1 = NEW PLOT, 2 = RETURN

SET HORIZONTAL SCALE? Y OR N=BLANK)

Y,
MIN-MAX X VALUES

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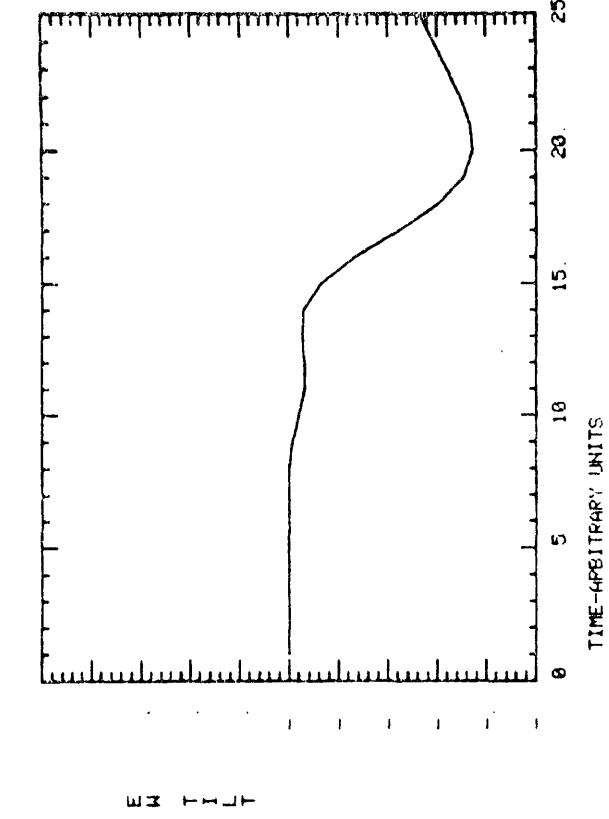
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LATERAL AND VERTICAL MIGRATION-CONSTANT SLIP



SET VERTICAL SCALE? Y OR N=BLANK)

Y,
MIN-MAX Y VALUES

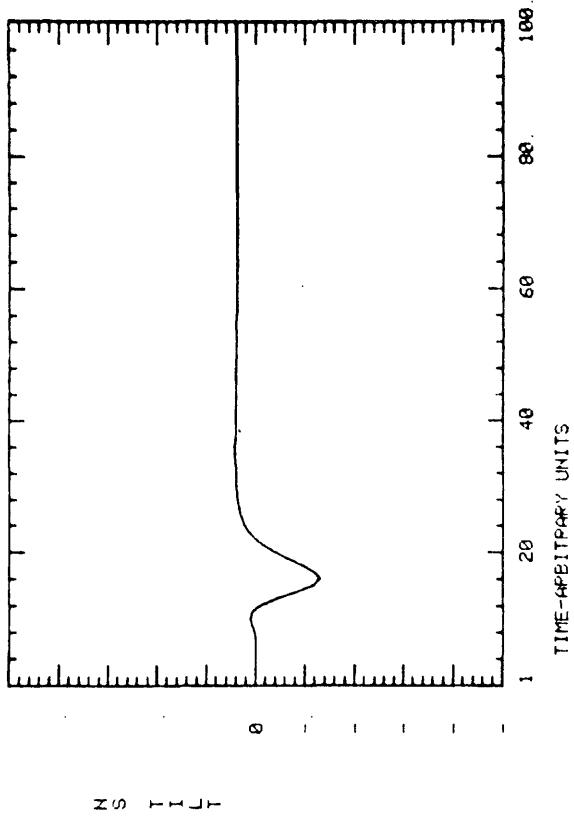
2,
2

SKIP PLOT OF FN TILT

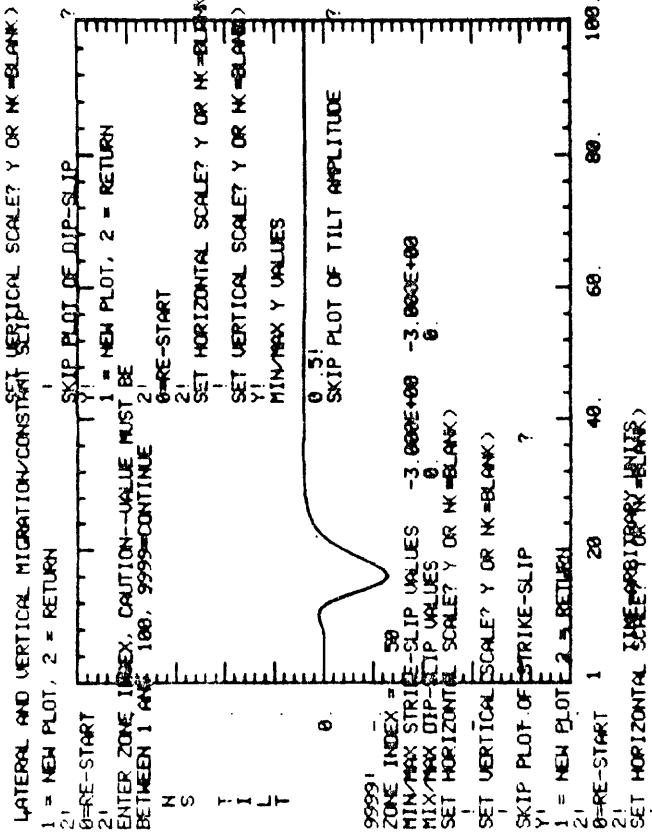
?


```
1 = NEW PLOT, 2 = RETURN  
2!  
RE-START  
SET HORIZONTAL SCALE? Y OR N (=BLANK)  
Y  
SET VERTICAL SCALE? Y OR N (=BLANK)  
Y  
MIN-MAX Y VALUES  
- 5 5  
SKIP PLOT OF NS TILT  
?
```

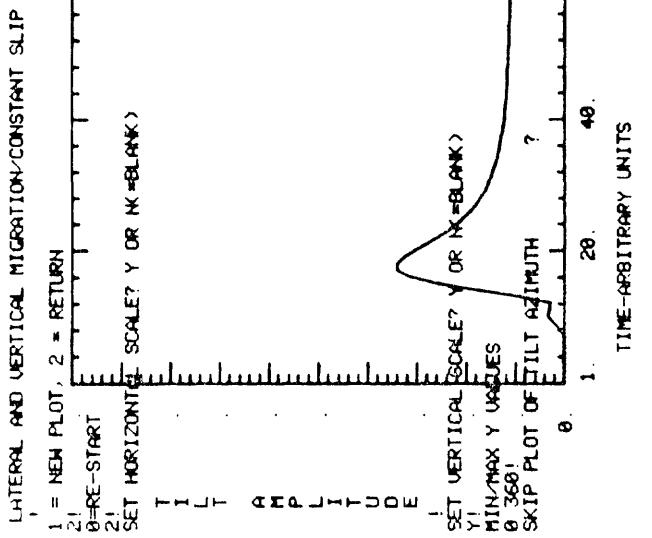
LATERAL AND VERTICAL MIGRATION/CONSTANT SLIP



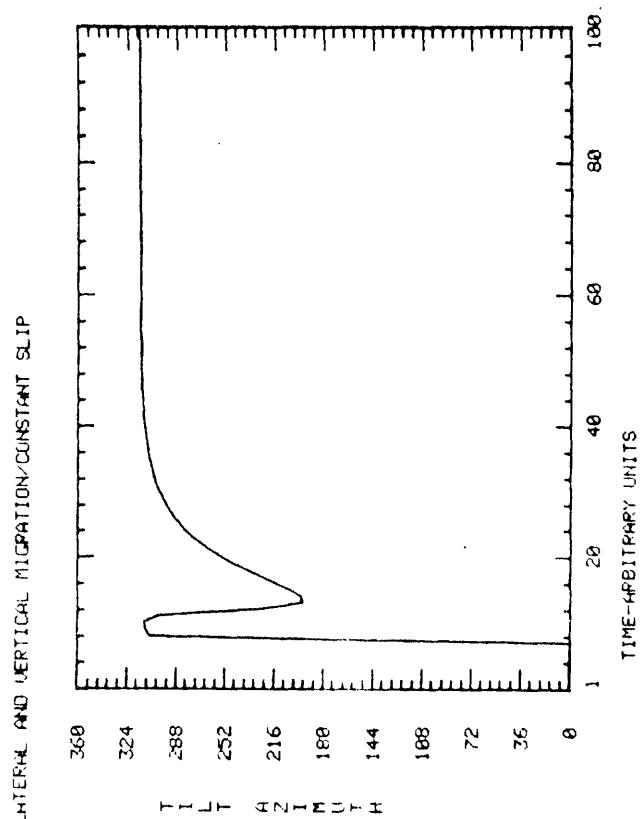
2-26



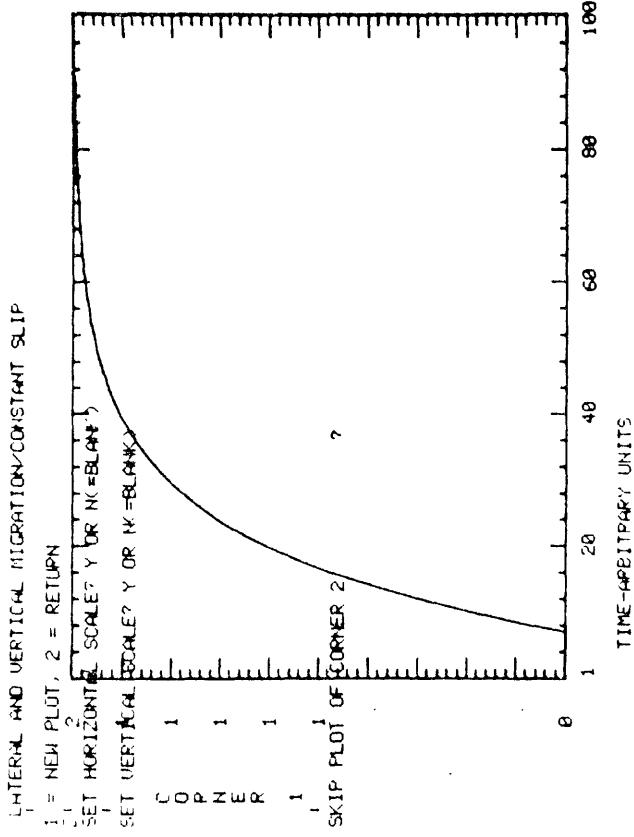
2-27



LATERAL AND VERTICAL MIGRATION/CONSTANT SLIP

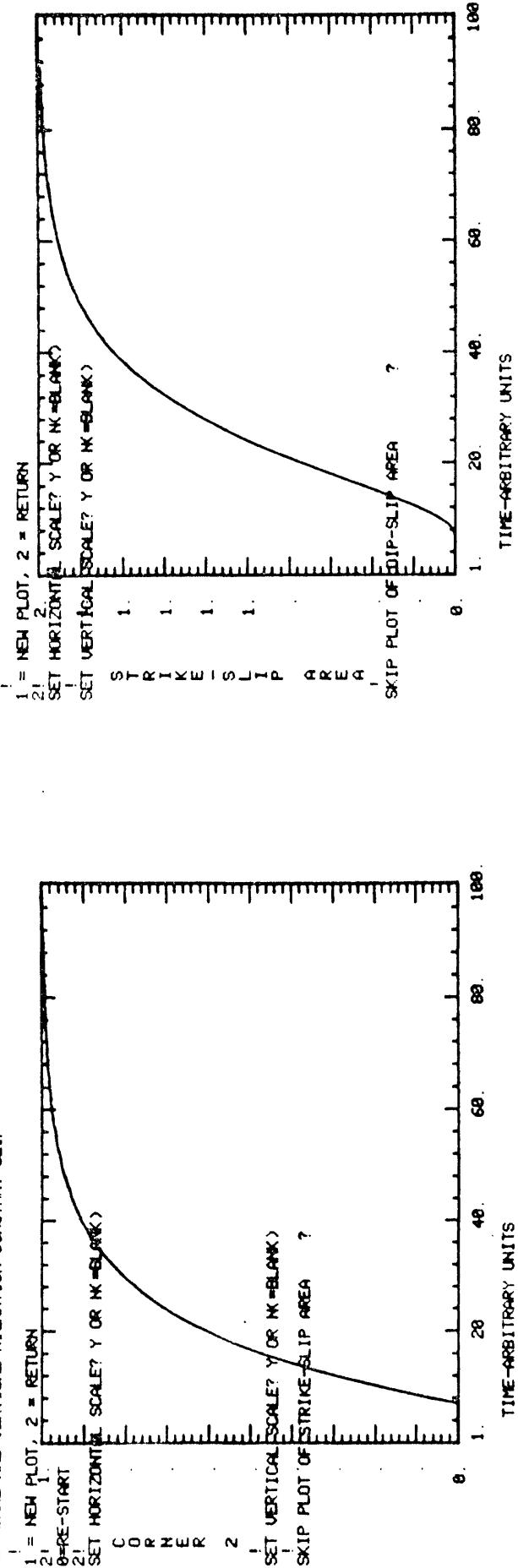


LATERAL AND VERTICAL MIGRATION/CONSTANT SLIP



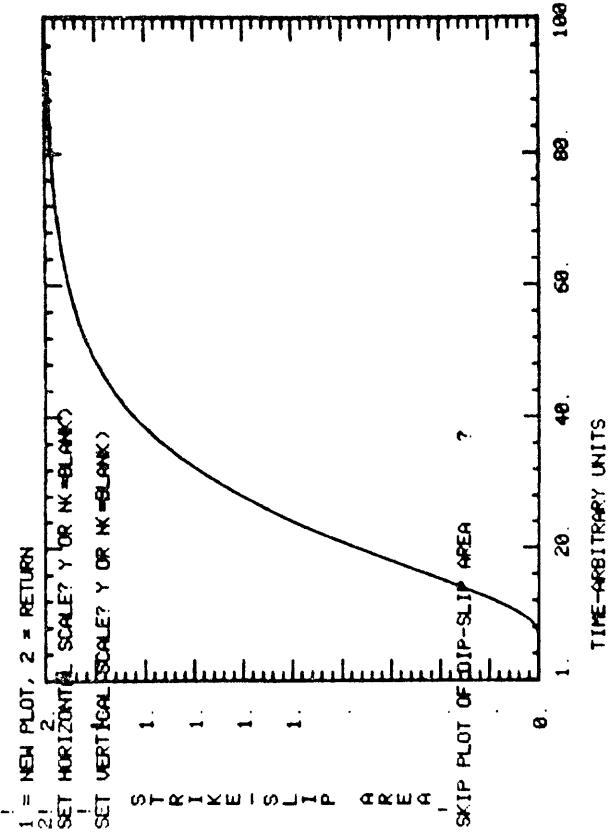
2-30

LATERAL AND VERTICAL MIGRATION-CONSTANT SLIP

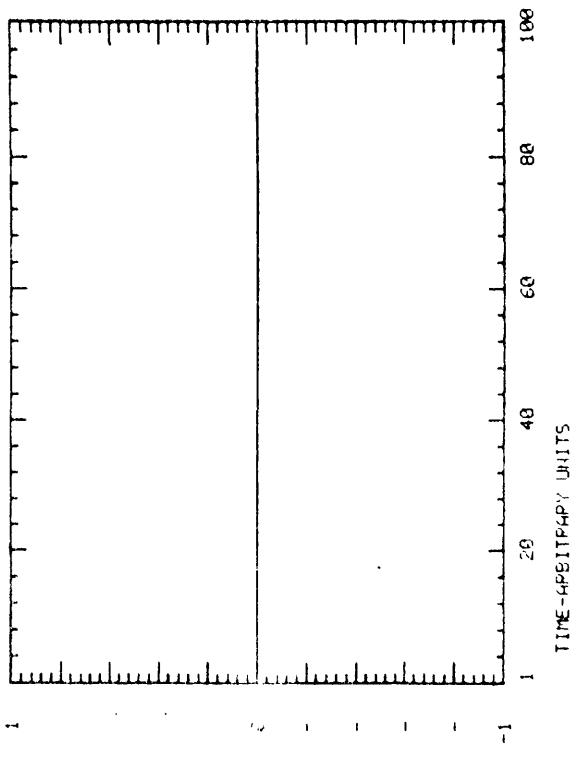


2-31

LATERAL AND VERTICAL MIGRATION-CONSTANT SLIP



LATERAL AND VERTICAL MIGRATION/CONSTANT SLIP



1 = NEW PLOT, 2 = RETURN

15-341

1=ZONE EXPANDS, 2=ZONE CONTRACTS
 1,2=SLIP INCREMENTED EXPONENTIALLY/LINEARLY
 STRIKE-SLIP/DIP-SLIP
 1,1
 0=INCREMENT CORNERS SEPARATELY
 1,2=INCREMENT ALL CORNERS EXPONENTIALLY/LINEARLY
 STRIKE-SLIP/DIP-SLIP
 0,0
 1=INCREMENTABLE INCREMENTED EXPONENTIALLY
 2=INCREMENTABLE INCREMENTED LINEARLY
 D1X1, D1X3, D2X3, D3X1
 1,2,1,2
 C1X1, C1X3, C2X3, C3X1
 2,1,2,1,1
 'U1>0' = LEFT-LATERAL STRIKE-SLIP
 'U2>0' = 'X2>0' SIDE DOWN
 U1FN, U1IN, U3IN, U3FN
 0,-3,0,1
 'TRIGGER' OPTION DESIRED?
 Y!
 0 = D(I1) > C(I2), 1 = D(I1) < C(I2)
 0!
 0 = STRIKE-SLIP/1 = DIP-SLIP ZONE TRIGGERED
 1!
 SPECIFY 11 AND 12
 9,5!
 C1X1IN C1X3IN, C2X3IN, C3X1IN, C1X1FN, C1X3FN, C2X3FN, C3X1FN
 0,0,2,0,1,0!
 D1X1IN, D1X3IN, D2X3IN, D3X1IN, D1X1FN, D1X3FN, D2X3FN, D3X1FN
 5,0,9,5,1,5,0,1,5!
 ENTER STATION COORDINATES--(X1,X2,
 1,5

```

! SPECIFY 2 CORNERS OF DISLOCATION SURFACE FOR DISPLAY
  1=0,1X1=0,2X1
  2=D1X3=D4X3
  5=0,3X1=D4X1
  9=C1,X1=1,2X1
  10=C3X3=C4X3
  13=C3X1=C4X1
  1,5!
  1 TO DISPLAY SLIP AS A FUNCTION OF TIME
  ENTER ZONE INDEX, CAUTION---  

  INDEX MUST BE BETWEEN 1 AND 100
  50!
  THETA=ANGLE BETWEEN STRIKE OF FAULT
  AND NORTH = 45 DEGREES
  MIN-MAX VALUES OF EW COMPONENT -3.37E-01 0
  MIN-MAX VALUES OF NS COMPONENT -2.93E-01 5.152E-03
  MIN-MAX VALUES OF AMPLITUDE 0 4.343E-01
  MIN-MAX VALUES OF AZIMUTH 8 318.863
  (NOTE--TILT AMPLITUDES ARE IN MICRORADIAN,  

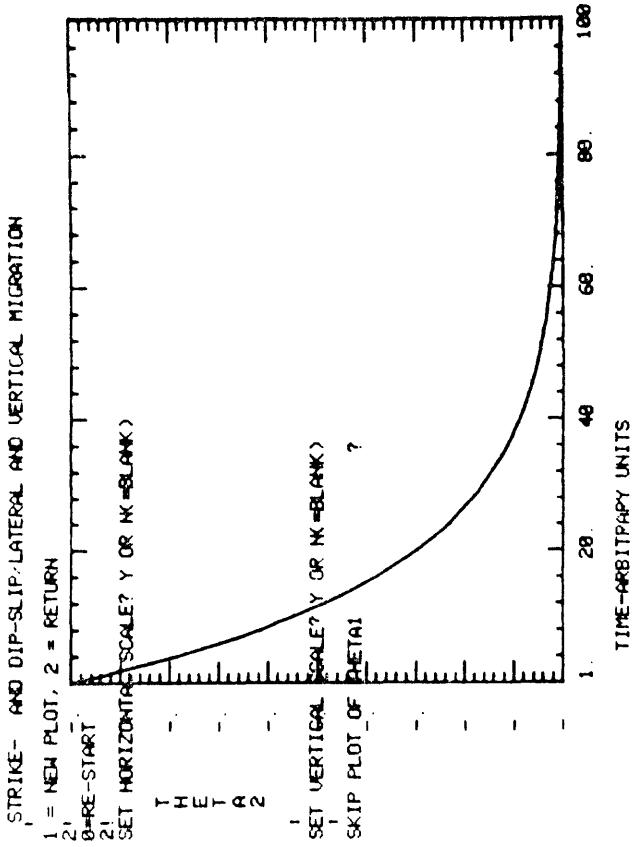
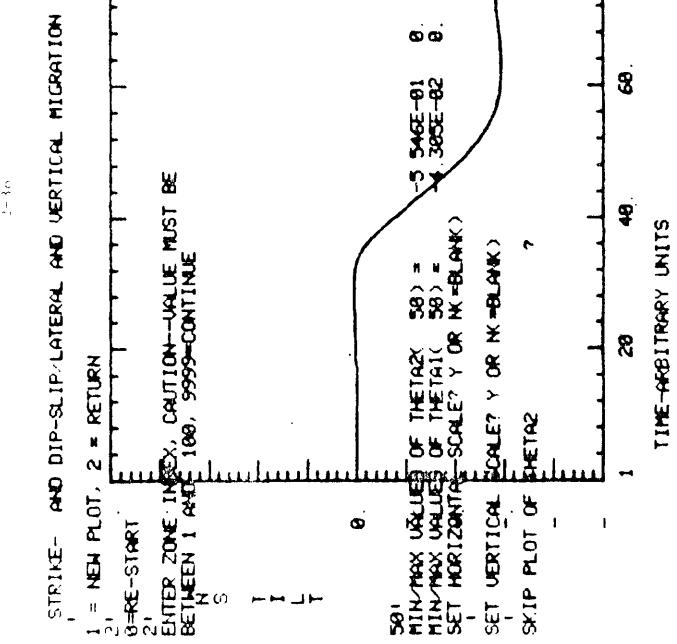
  AZIMUTH IN DEGREES)
  THE FOLLOWING ARE PLOTS OF THE EW AND NS COMPONENTS
  OF TILT, AND THE TILT AMPLITUDE
  AND AZIMUTH (MEASURE CLOCKWISE FROM NORTH).
  0=PL-START, 1=CONTINUE
  1!  

  WRITE PLOT TITLE, 80 CHARACTERS
  SET TILT, DIP-SLIP/LATERAL AND VERTICAL MIGRATION!
  SET HORIZONTAL SCALE? Y OR N=BLANK
  SET VERTICAL SCALE? Y OR N=BLANK
  Y!  

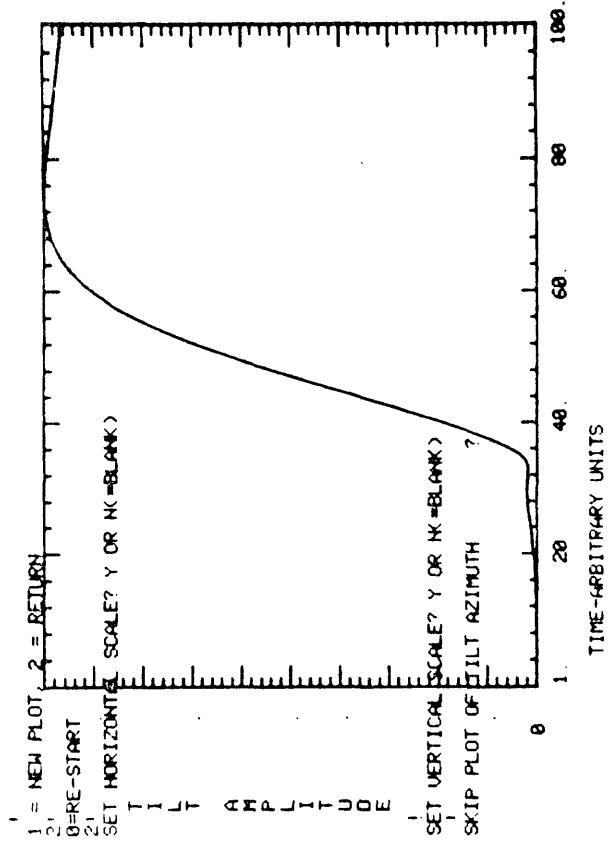
  MIN-MAX Y VALUES
  -5 5!  

  SIFT PLOT OF EW TILT
  ?  

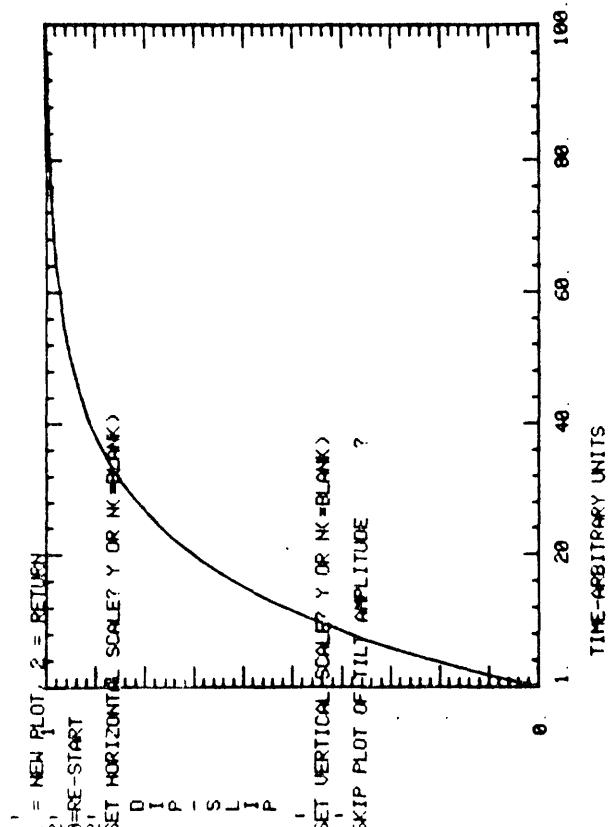

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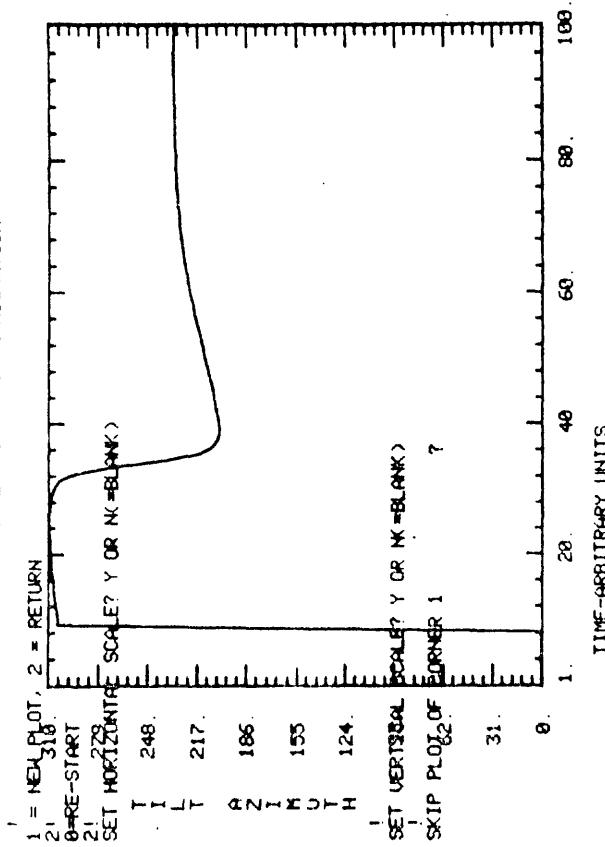
STRIKE- AND DIP-SLIP/LATERAL AND VERTICAL MIGRATION



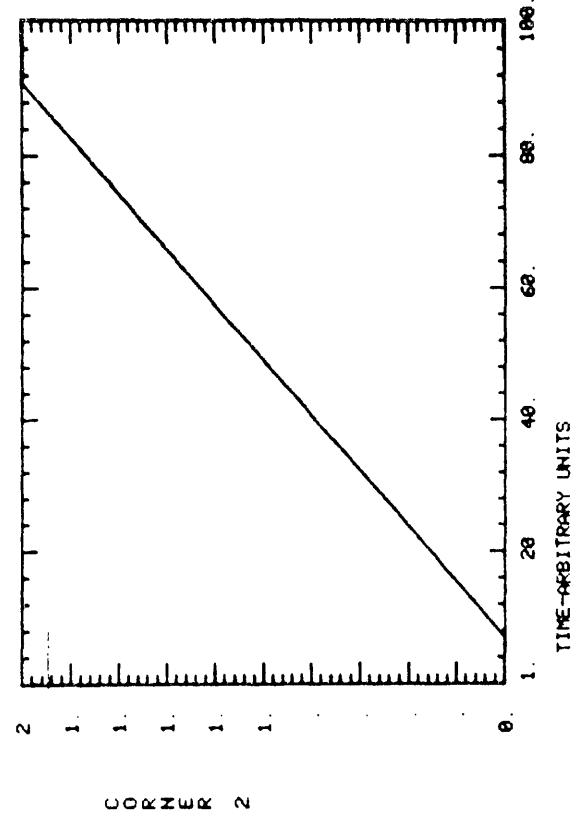
STRIKE- AND DIP-SLIP/LATERAL AND VERTICAL MIGRATION

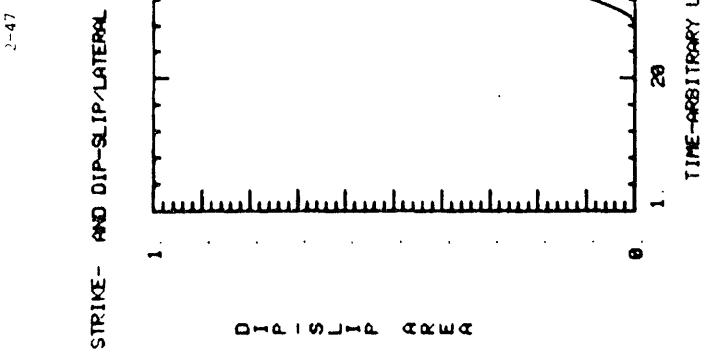
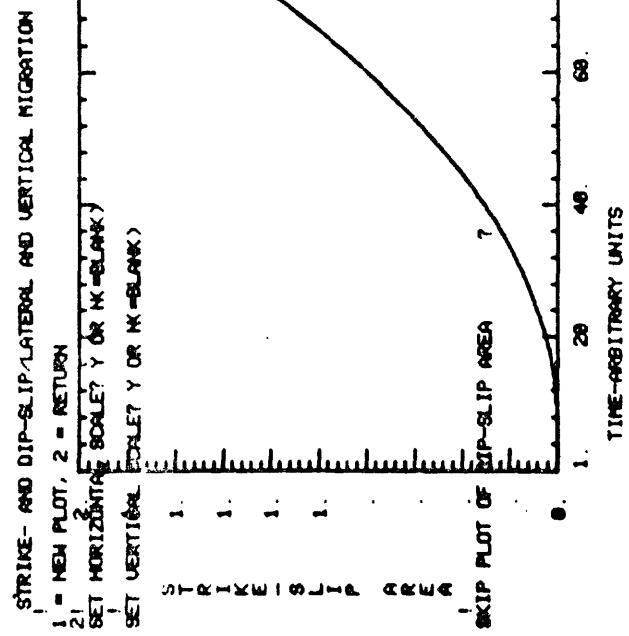


STRIKE- AND DIP-SLIP/LATERAL AND VERTICAL MIGRATION



STRIKE- AND DIP-SLIP/LATERAL AND VERTICAL MIGRATION





1 = NEW PLOT, 2 = RETURN
2 = RE-START

1=ZONE EXPANDS, 2=ZONE CONTRACTS
 1 1!
 1 1! 1-2-SLIP INCREMENTED EXPONENTIALLY/LINEARLY
 STRIKE-SLIP-DIP-SLIP
 1 1!
 0 = INCREMENT CORNERS SEPARATELY
 1 1! 1-INCREMENT ALL CORNERS EXPONENTIALLY/LINEARLY
 STRIKE-SLIP-DIP-SLIP
 0 0!
 1=PARTRIDGE INCREMENTED EXPONENTIALLY
 2=PARTRIDGE INCREMENTED LINEARLY
 01X1, 01X3, 02X3, 03X1
 1 2 1
 C1X1, C1X3, C2X3, C3X1
 2 1 2 1!
 'U1X8' = LEFT-LATERAL STRIKE-SLIP
 'U3X8' = 'X2X8 SIDE DOWN
 U1IN, U1FN, U3IN, U3FN
 0 -3 0 0!
 'TRIGGER' OPTION DESIRED?
 Y!
 0 = DX(11) > CC(12), 1 = DK(11) < CC(12)
 0 0!
 0 = STRIKE-SLIP1 = DIP-SLIP ZONE TRIGGERED
 1 1!
 SPECIFY 11 AND 12
 9 5!
 CX1IN, CX13IN, CX2X3IN, C3X1IN, C1X1FN, C1X3FN, C2X3FN,
 0 0 0 0 0 1 0!
 ENTER STITCH COORDINATES--(X1, Y2)

1. SPECIFY 2 CORNERS OF DISLOCATION SURFACE FOR DISPLAY
 1=0.1X1=0.2X1 2=0.1X1=0.4X3
 4=0.2X3=0.3X3 5=0.1X1=0.4X1
 9=C1X1=0.2X1 10=0.3X3=0.4X3
 12=C2X2=C3X3 13=C3X1=C4X1
 1.12.
 TO DISPLAY SLIP AS A FUNCTION OF TIME
 ENTER ZONE INDEX. CAUTION—
 INDEX MUST BE BETWEEN 1 AND 100
 33.
 THE TRENCHES BETWEEN STRIKE OF FAULT
 AND NORTH = 45 DEGREES
 MIN/MAX VALUES OF EW COMPONENT -9.785E-02 0
 MIN/MAX VALUES OF NS COMPONENT -7.035E-02 2.708E-02
 MIN/MAX VALUES OF AMPLITUDE 0 1
 MIN/MAX VALUES OF AZIMUTH 0 1.675E-01
 (NOTE—TILT AMPLITUDES ARE IN MICRODEGREES,
 AZIMUTH IN DEGREES)
 THE FOLLOWING ARE PLOTS OF THE EW AND NS COMPONENTS
 OF TILT, AND THE TILT AMPLITUDE
 AND AZIMUTH (MEASURE CLOCKWISE FROM NORTH).
 1.
 WRITE PLOT TITLE, 80 CHARACTERS
 SAME VALUES AS PREVIOUS CASE, EXCEPT THAT DIP-SLIP=0.0!
 1.
 SET HORIZONTAL SCALE? Y OR N=BLANK
 Y
 MIN/MAX Y VALUES
 -2 2
 SKIP PLOT OF EW TILT
 ?
 1.
 SET VERTICAL SCALE? Y OR N=BLANK
 Y
 MIN/MAX Y VALUES
 -2 2
 SKIP PLOT OF NS TILT
 ?
 1.
 SET HORIZONTAL SCALE? Y OR N=BLANK
 Y
 MIN/MAX X VALUES
 1 200 400 600 800 1000
 TIME=ARBITRARY UNITS

SOME USES AS PREVIOUS CASE, EXCEPT THAT DIP-SLIPPE 6

SAME VALUES AS PREVIOUS CASE, EXCEPT THAT DIP-SLIP=0
 1 = NEW PLOT, 2 = RETURN
 21 RE-START
 21 ENTER ZONE INDEX, CAUTION--VALUE MUST BE
 BETWEEN 1 AND 100, 9999=CONTINUE
 S
 1
 L
 T
 SPACES
 ZONE INDEX = 33
 MIN MAX STRIKE-SLIP VALUES -2.993E-03
 MIX MAX DIP-SLIP VALUES 6.
 SET HORIZONTAL SCALE? Y OR N (ENTER)
 SET VERTICAL SCALE? Y OR N (ENTER)
 SKIP PLOT OF STRIKE-SLIP ?
 Y
 1 = NEW PLOT
 21 RE-START
 SET HORIZONTAL SCALE? Y OR N (ENTER)
 SET VERTICAL SCALE? Y OR N (ENTER)

SAME VALUES AS PREVIOUS CASE, EXCEPT THAT DIP-SLIP=0

1 = NEW PLOT, 2 = RETURN

2 = PRE-START

SET HORIZONTAL SCALE?

SET VERTICAL SCALE? Y OR N <BLANK>

MIN-MAX Y VALUES

0-358!

SKIP PLOT OF TILT AZIMUTH

TIME - ARBITRARY UNITS

TIME-ARBITRARY UNITS

1

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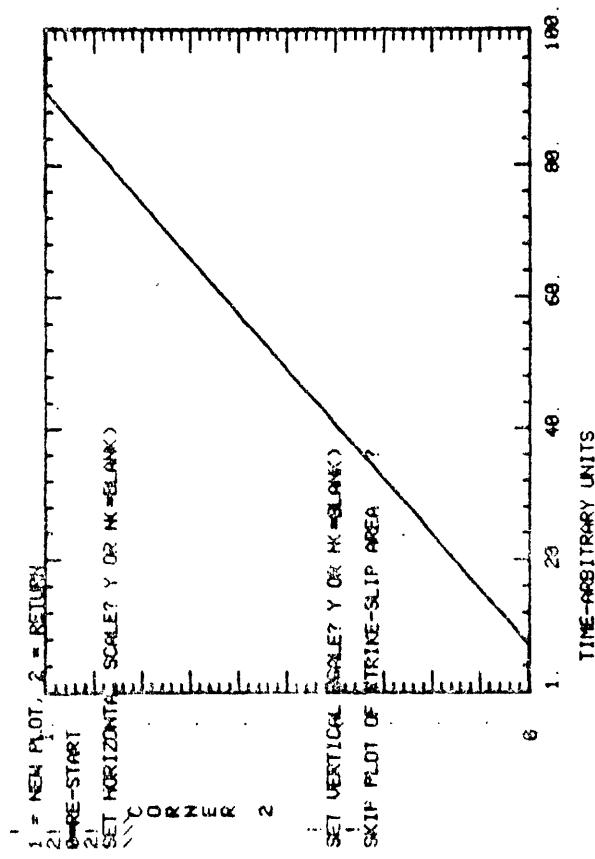
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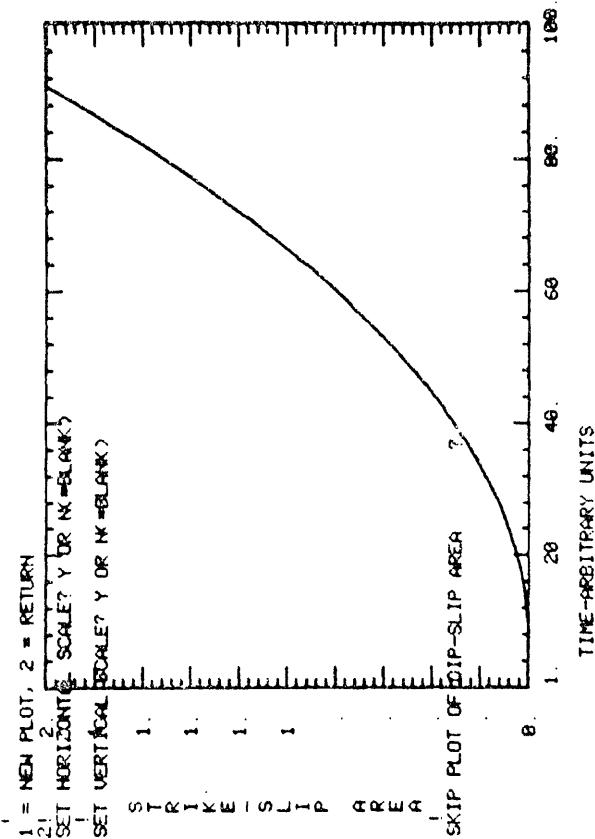
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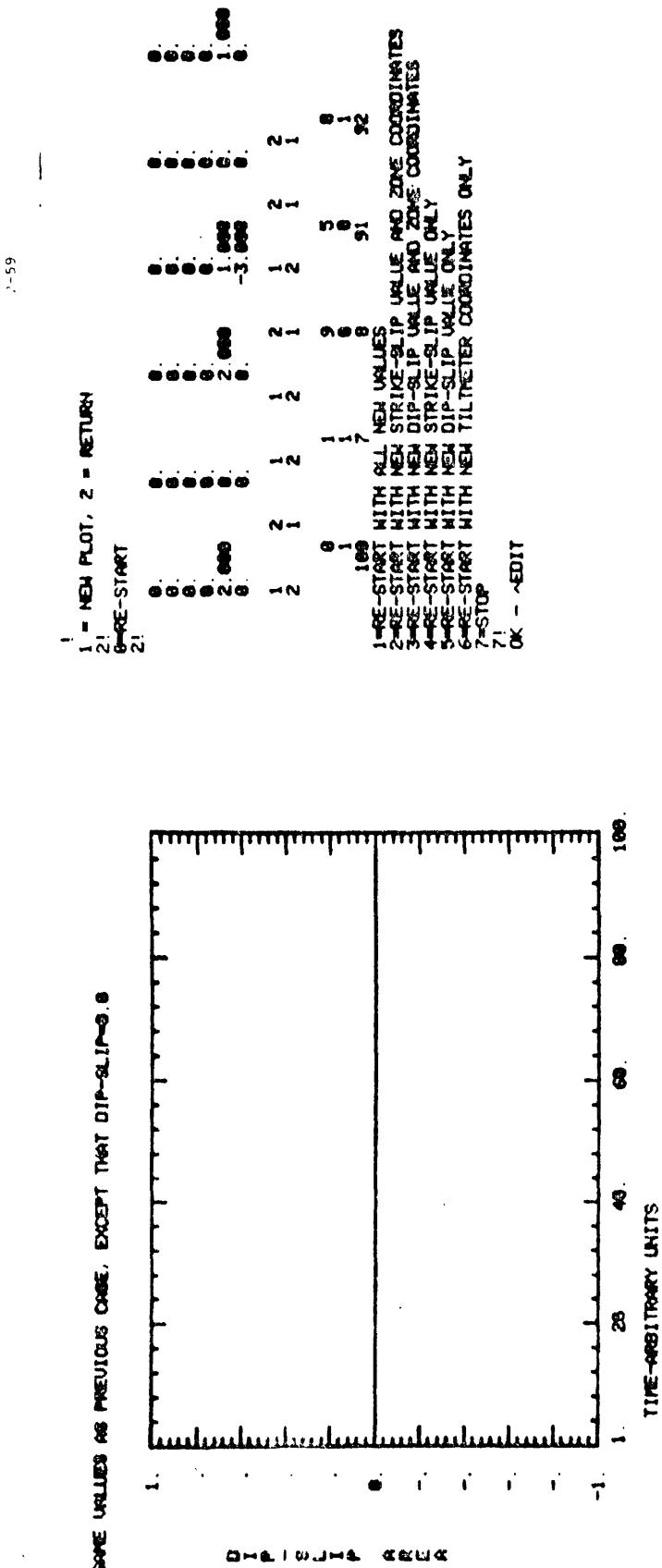
0

SAME VALUES AS PREVIOUS CASE, EXCEPT THAT DIP-SLIP=0



SAME VALUES AS PREVIOUS CASE, EXCEPT THAT DIP-SLIP=0





PROGRAM LISTING FOR SLPPRP

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1  DELETE(LGO,OUTFUT,SLPPRP)
2  SLPPRP.
3  CXIT.
4  LINECOPY(GRAPHIC,TXLGO/RN,TXLGO)
5  LINECOPY(JCRAT,NPLGC/RN,NPLGO)
6  DELLTE(LGC,OUTPLT,SLPPRP)
7  RUN7c(S)
8  LINK(F=LGO,F=TXLGO,F=NPLGO,B=SLPPRP)
9  SLPPRP.
10 FIN.
11 EOF
12      PROGRAM SLPPRP(TAPETTY=201,FILM=TAPETTY,TAPE7=TAFETTY)
13 COMMON/TVPUCI/TVPUL(8)
14 COMMON/TVTUNE/ITUNE(30)
15 COMMON/JFLCT/XLT,XRT,YLC,YLP,MAJX,MAJY,KX(2),KY(2),
16 LTITLE(8),LC,LTF,LNLGX,LNLGY,NCLX,NCLY,LTITLE2(8)
17 DIMENSION IFET(8)
18 DIMENSION TX(100),TY(100),T(100),CORNRI(100),CORNRI2(100)
19 DIMENSION C(20),C(40),A(30),IT(4),ICFNRI(16),STSLIP(100)
20 DIMENSION CIPSLP(100),SSAREA(100),USAREA(100)
21 DIMENSION THETA1(100,100),THETA2(100,100)
22 DIMENSION TAMP(100),TAZM(100)
23 CALL FET(ELTAPE7,IFET,o)
24 IFET(2)=IFET(2).OR.0000 0010 0000 0000 0000B
25 IFET(8)=IFET(8).OR.4000 0000 0000 0000 0000B
26 CALL FET(ELTAPE7,IFET,-8)
27      DC 101 J=1,18
28      BC(J)=0. BC(J+18)=0. BC(J)=0.
29 101 CONTINUE
30      K=ITE(7,1)
31      1 FORMAT(*1=ZONE EXPANDS, 2=ZONE CONTRACTS*)
32      CALL GETNUM(A) $IFLAG=A(1) $WRITE(7,2)
33      2 FORMAT(*1/2=SLIP INCREMENTED EXPONENTIALLY/LINEARLY*,/,
34      1      *STRIKE-SLIP/CIF-SLIP*)
35      CALL GETNUM(A) $KFLAGS=A(1) $KFLAGU=A(2) $WRITE(7,3)
36      3 FORMAT(*0 =INCREMENT CORNERS SEPARATELY*,/,
37      1      *1/2=INCREMENT ALL CORNERS EXPONENTIALLY/LINEARLY*,/,
38      1      *STRIKE-SLIP/CIF-SLIP*)
39      CALL GETNUM(A) $LFLAG=A(1) $MFLAG=A(2)
40      DO 110 I=1,4
41      IT(I)=5
42 110 CONTINUE
43      DO 4 I=1,16
44      + ICNR(I)=1
45      IF (LFLAG.LQ.0.OR.MFLAG.EQ.0)CALL SLPCRN(LFLAG,MFLAG,ICNR)
46      IF (LFLAG.EQ.2)GOTO 5 $GOTO6
47      5 DO 7 I=9,16
48      7 ICNR(I)=2
49      6 IF (MFLAG.EC.2)GOTO8 $GOTO9
50      5 DC 10 I=1,8
51      10 ICNR(I)=2
52      9 WRITE(7,11) $CALL GETNUM(A) BC(33)=A(1) BC(34)=A(2)
53      11 FORMAT(*'U1>0' = LEFT-LATERAL STRIKE-SLIP*,/,
54      1      *'U3>0' = 'X2>0' SIDE DOWN*,/,
55      1      *U1IN, J1FN, U3IN, U3FN*)
56      C(35)=A(3) BC(36)=A(4) $WRITE(7,12)
57      12 FORMAT(*'TRIGGER' OPTION DESIRED?*)
58      FLAL(7,13)TRIG LIF(TRIG.EG.1HY)CALL TRIGGR(IT)

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59      13 FORMAT(A1)
60      IF(C(33).EQ.0..AND.C(34).EQ.0.)GOTO14
61      WRITE(7,15) &CALL GETNUM(A) &C(17)=C(19)=A(1)
62      15 FORMAT(*C1X1IN,C1X3IN,C2X3IN,C3X1IN,C1X1FN,C1X3FN,C2X3FN,C3X1FN*)
63      C(18)=C(24)=A(2) &C(20)=C(22)=A(3) &C(21)=C(23)=A(4)
64      C(25)=C(27)=A(5) &C(26)=C(32)=A(6) &C(28)=C(30)=A(7)
65      C(29)=C(31)=A(8)
66      14 IF(C(35).EQ.0..AND.C(36).EQ.0.)GOTO16
67      WRITE(7,17) &CALL GLTNUM(A) &C(1)=C(3)=A(1) &C(2)=C(8)=A(2)
68      17 FORMAT(*D1X1IN,D1X3IN,D2X3IN,D3X1IN,D1X1FN,D1X3FN,D2X3FN,D3X1FN*)
69      C(4)=C(6)=A(3) &C(5)=C(7)=A(4) &C(9)=C(11)=A(5)
70      C(10)=C(16)=A(6) &C(12)=C(14)=A(7) &C(13)=C(15)=A(8)
71      16 WRITE(7,18) &CALL GETNUM(A) &X1=A(1) &X2=A(2)
72      18 FORMAT(*ENTER STATION COORDINATES--(X1,X2)*)
73      X3=C. &NRECPT=100 &N=(.075*NRECPT) &NSLPP=NRECPT
74      N1=N+1 &N2=NRECPT-(.075*NRECPT)-1
75      N3=N2+1 &THETA=45. &PI=3.1415926 &WRITE(7,30)
76      FNSLPP=NSLPP &RN1=N1 &RN2=N2 &ONE=1. &ITIME=99999
77      30 FORMAT(*SPECIFY 2 CORNERS OF DISLOCATION SURFACE FOR DISPLAY*,/,,
78      1 * 1=D1X1=D2X1           2=D1X3=D4X3*,/,,
79      1 * 4=D2X3=D3X3           5=D3X1=D4X1*,/,,
80      1 * 9=C1X1=C2X1           10=C3X3=C4X3*,/,,
81      1 * 12=C2X3=C3X3          13=C3X1=C4X1*)
82      CALL GETNUM(A) &M1=A(1) &M2=A(2)
83      WRITE(7,113)NRECPT &CALL GETNUM(A) &INDEX=A(1)
84      113 FORMAT(*TO DISPLAY SLIP AS A FUNCTION OF TIME*,/,,
85      1       *ENTER ZONE INDEX, CAUTION---*,/,,
86      1       *INDEX MUST BE BETWEEN 1 AND *,I4)
87      75 CONTINUE
88      DO 21 J=1,3
89      C(J)=C(J) &D(J+3)=C(J+1E)
90      21 CONTINUE
91      C(17)=C(33) &D(18)=C(35)
92      DO 13 I=1,N
93      T(I)=I
94      22 DO 63 K=1,NSLPP
95      CALL CMPTLT(D,X1,X2,X3,T1,T2)
96      THETA1(I,K)=T1 &THETA2(I,K)=T2
97      IF(I.EQ.INDEX)STSLP(K)=C(17) &IF(I.EQ.INDEX)DIPSLP(K)=D(18)
98      63 CONTINUE
99      CURNR1(I)=D(M1) &CCRNR2(I)=D(M2)
100     SSAREA(I)=A3S((D(15)-D(9))*(D(12)-D(10)))
101     DSAREA(I)=A3S((D(7)-D(1))*(D(4)-D(2)))
102     19 CONTINUE
103     DO 24 J=1,8
104     C(J)=C(J+8) &D(J+8)=C(J+24)
105     24 CONTINUE
106     C(17)=C(34) &D(18)=C(36)
107     DO 23 I=N3,NRECPT
108     T(I)=I
109     DO 64 K=1,NSLPP
110     RK=E &CALL XPNSHL(C(33),C(34),ONE,RNSLPP,RK,Y1)
111     CALL XPNSHL(C(35),C(36),ONE,RNSLPP,RK,Y2)
112     IF(KFLAGS.NE.1)CALL ALINAR(C(33),C(34),ONE,RNSLPP,RK,Y1)
113     IF(KFLAG.E.NE.1)CALL ALINAR(C(35),C(36),ONE,RNSLPP,RK,Y2)
114     D(17)=Y1 &D(18)=Y2
115     CALL CMPTLT(D,X1,X2,X3,T1,T2)
116     THETA1(I,K)=T1 &THETA2(I,K)=T2

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117      IF(I.EQ.INDEX)STSLIP(K)=0(17) $IF(I.EQ.INDEX)DIPSLP(K)=0(18)
118      04 CONTINUE
119      CURNR1(I)=0(M1) $CCKNR2(I)=0(M2)
120      SSAREA(I)=ABS((0(15)-0(9))*0(12)-0(10)))
121      LSAREA(I)=ABS((L(7)-0(1))*(0(+)-0(2)))
122      23 CONTINUE
123      IFGKREC=0
124      GO 25 I=N1,N2
125      T(I)=I $RI=I
126      DO 05 K=1,NSLPPT
127      RK=K
128      IF(TKIG.EQ.1HY)GOTO26
129      GO 27 J=1,t
130      JB=J+4 $A1=C(J) $B=C(J8) $E=C(J8+8) $F=C(J+24)
131      CALL XPNSHL(A1,B,RN1,RN2,RI,Y1)
132      CALL XPNSHL(E,F,RN1,RN2,RI,Y2)
133      IF(ICRNR(J).EQ.2)CALL ALINAR(A1,B,RN1,RN2,RI,Y1)
134      IF(ICRNR(J8).EQ.2)CALL ALINAR(E,F,RN1,RN2,RI,Y2)
135      C(J)=Y1 $D(J8)=Y2
136      27 CONTINUE
137      CALL XPNSHL(C(33),C(34),ONE,RNSLPP,RK,Y1)
138      CALL XPNSHL(C(35),C(36),ONE,RNSLPP,RK,Y2)
139      IF(KFLAGS.NE.1)CALL ALINAR(C(33),C(34),ONE,RNSLPP,RK,Y1)
140      IF(KFLAGS.NE.1)CALL ALINAR(C(35),C(36),ONE,RNSLPP,RK,Y2)
141      L(17)=Y1 $D(15)=Y2 GOTO28
142      28 IF(.LT.(2).EG.1.AND.KFLAGS.EQ.1)CALL XPNSHL(C(33),C(34),ONE,
143      1 RNSLPP,RK,Y)
144      IF(IT(2).EG.1.AND.KFLAGS.NE.1)CALL ALINAR(C(33),C(34), ONE,
145      1 RNSLPP,RK,Y)
146      IF(IT(2).EG.0.AND.KFLAGC.EG.1)CALL XPNSHL(C(35),C(36),ONE,
147      1 RNSLPP,RK,Y)
148      IF(IT(2).EQ.0.AND.KFLAGD.NE.1)CALL ALINAR(C(35),C(36),ONE,
149      1 RNSLPP,RK,Y)
150      IF(IT(2).EG.0)D(18)=Y $IF(IT(2).EQ.1)D(17)=Y
151      GO 32 J=1,t
152      JB=J+8 $A1=C(J) $B=C(J8) $E=C(J8+8) $F=C(J+24)
153      CALL XPNSHL(A1,B,RN1,RN2,RI,Y1)
154      CALL XPNSHL(E,F,RN1,RN2,RI,Y2)
155      IF(ICRNR(J).EQ.2)CALL ALINAR(A1,B,RN1,RN2,RI,Y1)
156      IF(ICRNR(J8).EQ.2)CALL ALINAR(E,F,RN1,RN2,RI,Y2)
157      L(J)=Y1 $U(J8)=Y2
158      32 CONTINUE
159      MIT3=IT(3) $MIT4=IT(4) $IF(IT(1).EQ.1)GOTC29
160      IF(U(MIT3).LT.0(MIT4).AND.IT(2).EQ.0)D(17)=C(33)
161      IF(U(MIT3).LT.0(MIT4).AND.IT(2).EQ.1)D(18)=C(35)
162      IF(D(MIT3).LT.0(MIT4).AND.IT(2).EQ.1)GOT033
163      IF(U(MIT3).GE.0(MIT4))GOT035
164      GO 40 J=9,16
165      40 U(J)=C(J+8)
166      GOTC26
167      49 IF(D(MIT3).GT.0(MIT4).AND.IT(2).EQ.0)D(17)=C(33)
168      IF(D(MIT3).GT.0(MIT4).AND.IT(2).EQ.1)D(18)=C(35)
169      IF(D(MIT3).GT.0(MIT4).AND.IT(2).EQ.1)GOTC33
170      IF(D(MIT3).LE.0(MIT4))GOT035
171      GO 34 J=9,16
172      54 L(J)=C(J+8)
173      GOTC28
174      35 GO 36 J=1,t

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175      36 D(J)=C(J)
176      GO TO 28
177      35 IFGREC=IFGREC+1
178      IF(IFGREC.EQ.1)ITIME=I
179      IF(IFGREC.EQ.1)RITIME=ITIME
180      IF(IT(2).EQ.0.AND.KFLAGS.EQ.1)CALL XPNSHL(C(33),C(34),ONE,
181      1 RNSLPP,RK,Y)
182      IF(IT(2).EQ.0.AND.KFLAGS.NE.1)CALL ALINAR(C(33),C(34),ONE,
183      1 RNSLPP,RK,Y)
184      IF(IT(2).EQ.1.AND.KFLAGD.EQ.1)CALL XPNSHL(C(35),C(36),ONE,
185      1 RNSLPP,RK,Y)
186      IF(IT(2).EQ.1.AND.KFLAGD.NE.1)CALL ALINAR(C(35),C(36),ONE,
187      1 RNSLPP,RK,Y)
188      IF(IT(2).EQ.1)D(18)=Y $IF(IT(2).EQ.0)D(17)=Y
189      IF(IT(2).EQ.1)GOTO 37
190      DO 38 J=9,16
191      A1=C(J+8) $B=C(J+16) $CALL XPNSHL(A1,B,RITIME,RN2,RI,Y)
192      IF(ICRNR(J).EQ.2)CALL ALINAR(A1,B,RITIME,RN2,RI,Y)
193      38 D(J)=Y
194      GO TO 28
195      37 DO 39 J=1,8
196      E=C(J) $F=C(J+8) $CALL XPNSHL(E,F,RITIME,RN2,RI,Y)
197      IF(ICRNR(J).EQ.2)CALL ALINAR(E,F,RITIME,RN2,RI,Y)
198      39 U(J)=Y
199      28 CALL CMPTLT(D,X1,X2,X3,T1,T2)
200      THETA1(I,K)=T1 $THETA2(I,K)=T2
201      IF(I.EQ.INDEX)STSLIP(K)=D(17) $IF(I.EQ.INDEX)DIPSLP(K)=D(18)
202      45 CONTINUE
203      CORNR1(I)=D(M1) $CORNR2(I)=D(M2)
204      SSAREA(I)=ABS((D(15)-D(9))*(D(12)-D(10)))
205      LSAREA(I)=ABS((D(7)-D(1))*(D(4)-D(2)))
206      25 CONTINUE
207      DO 41 I=1,NRECPT
208      SUM11=SUM12=SUM21=SUM22=0.
209      DO 42 J=1,I
210      AT=THETA1(J,I+1-J) $B=THETA2(J,I+1-J) $SUM11=AT+SUM11
211      SUM21=B+SUM21
212      42 CONTINUE
213      LM=I-1 $IF(LM.LT.1)GOTO 43
214      DO 44 J=1,LM
215      AT=THETA1(J,I-J) $B=THETA2(J,I-J) $SUM12=AT+SUM12 $SUM22=B+SUM22
216      44 CONTINUE
217      43 TX(I)=SUM21-SUM22 $TY(I)=SUM11-SUM12
218      41 CONTINUE
219      IF(IFLAG.EQ.2)GOTO 46
220      AR=TX(1) $B=TY(1)
221      DO 47 I=1,NRECPT
222      TX(I)=TX(I)-AR
223      47 TY(I)=TY(I)-B
224      GOTO 48
225      40 DO 49 I=1,NRECPT
226      TX(I)=TX(NRECPT)-TX(I)
227      49 TY(I)=TY(NRECPT)-TY(I)
228      48 CT=COS(THETA*(PI/180.))
229      ST=SIN(THETA*(PI/180.))
230      DO 50 I=1,NRECPT
231      B=TX(I) $AR=TY(I)
232      TY(I)=AR*CT + B*ST $TX(I)=-AR*ST + B*CT

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233 TAMP(I)=SQR((TX(I)**2)+(TY(I)**2))
234 IF(TY(I).EQ.0.)TY(I)=1.E-20
235 TAZM(I)=(ATAN(TX(I)/TY(I)))*(180./PI)
236 IF(TY(I).LT.0.)TAZM(I)=TAZM(I)+180.
237 IF(TAZM(I).LT.0.)TAZM(I)=TAZM(I)+360.
238 IF(TAZM(I).GT.360.)TAZM(I)=TAZM(I)-360.
239 50 CONTINUE
240 WFILE(7,51)THEITA
241 51 FORMAT(*THEITA=ANGLE BETWEEN STRIKE OF FAULT*,/,
242      *AND NORTH = *,F10.3,* DEGREES*)
243 CALL AMINMX(TX,NRECPT,TXMIN,TXMAX)
244 CALL AMINMX(TY,NRECPT,TYMIN,TYMAX)
245 CALL AMINMX(TAMP,NRECPT,TAMPMN,TAMPMX)
246 CALL AMINMX(TAZM,NRECPT,TAZMMN,TAZMMX)
247 WRITE(7,51)TXMIN,TXMAX,TYMIN,TYMAX,TAMPMN,TAMPMX,TAZMMN,TAZMMX
248 51 FORMAT(*MIN/MAX VALUES OF EW COMPONENT*,2X,E10.3,2X,E10.3,/,,
249      *MIN/MAX VALUES OF NS COMPONENT*,2X,E10.3,2X,E10.3,/,,
250      *MIN/MAX VALUES OF AMPLITUDE*,5X,E10.3,2X,E10.3,/,,
251      *MIN/MAX VALUES OF AZIMUTH*,3X,F10.3,2X,F10.3,/,,
252      *(NOT--TILT AMPLITUDES ARE IN MICRORADIANS,*,/,,
253      *AZIMUTH IN DEGREES*)*
254 WRITE(7,52) 5CALL GETNUM(A) $IF(A(1).EQ.0.)GOTO100
255 52 FORMAT(*THE FOLLOWING ARE PLOTS OF THE EW AND NS COMPONENTS*,/,
256      *OF TILT, AND THE TILT AMPLITUDE*,/,,
257      *AND AZIMUTH (MEASURE CLOCKWISE FROM NORTH)*,/,,
258      *0=RE-START, 1=CONTINUE*)
259 LU=7 BLNLGX=1 BLNLGY=1 INCLX=2 INCLY=2
260 LU 20L KME=1,9
261 200 LTITL2(K1)=10H
262 WRITE(7,53) 5PAU(7,54)(LTITL(I),I=1,8)
263 53 FORMAT(*WRITE PLOT TITLE, 80 CHARACTERS*)
264 54 FORMAT(BA10)
265 MAJX=5 MAJY=10 BKTER1=10HEW TILT      BKTER2=10H
266 CALL AGRAPF(TX,T,TXMIN,TXMAX,NRECPT,KTER1,KTER2)
267 WRITE(7,55) 5CALL GETNUM(A) $IF(A(1).EQ.0.)GOTO100
268 55 FORMAT(*0=RE-START*)
269 KTER1=10HNS TILT      BKTER2=10H
270 CALL AGRAPF(TY,T,TYMIN,TYMAX,NRECPT,KTER1,KTER2)
271 WRITE(7,55) 5CALL GETNUM(A) $IF(A(1).EQ.0.)GOTO100
272 KTER1=10HTHETA2
273 56 WRITE(7,57)NSLPPT
274 57 FORMAT(*ENTER ZONE INDEX, CAUTION--VALUE MUST BE*,/,,
275      *BETWEEN 1 AND *,I4,*, 9999=CONTINUE*)
276 CALL GETNUM(A) $I=A(1) $IF(I.EQ.9999)GOTC58
277 IF(I.GT.1.NSLPPT)GOTC56 $IKJ=I
278 IJ 59 K=1,NSLPPT
279 TY(K)=THETA1(IKJ,K)
280 58 TX(K)=THETA2(IKJ,K)
281 CALL AMINMX(TX,NSLPPT,TXMIN,TXMAX)
282 CALL AMINMX(TY,NSLPPT,TYMIN,TYMAX)
283 WRITE(7,60)IKJ,TXMIN,TXMAX,IKJ,TYMIN,TYMAX
284 60 FORMAT(*MIN/MAX VALUES OF THETA2(*,I4,*) = *,5X,E10.3,2X,E10.3,/
285      *MIN/MAX VALUES OF THETA1(*,I4,*) = *,5X,E10.3,2X,E10.3)
286 CALL AGRAPF(TX,T,TXMIN,TXMAX,NSLPPT,KTER1,KTER2)
287 WRITE(7,60) 5CALL GETNUM(A) $IF(A(1).EQ.0.)GOTO100
288 KTER1=10HTHETA1
289 CALL AGRAPF(TY,T,TYMIN,TYMAX,NSLPPT,KTER1,KTER2)
290 WRITE(7,60) 5CALL GETNUM(A) $IF(A(1).EQ.0.)GOTO100

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291      GO TO 56
292      58 CALL AMINMX(STSLIP,NSLFPT,SSMIN,SSMAX)
293      CALL AMINMX(DIPSLP,NSLFFT,DSMIN,DSMAX)
294      WRITE(7,114) INDEX,SSMIN,SSMAX,DSMIN,DSMAX
295      114 FORMAT(*ZONE INDEX = *,I4,/,
296           1      *MIN/MAX STRIKE-SLIP VALUES *,2X,E10.3,2X,E10.3,/,
297           1      *MIX/MAX DIP-SLIP VALUES *,5X,E10.3,2X,F10.3)
298      KTER1=10H STRIKE-SLI $KTER2=10HP
299      CALL AGRAPH(STSLIP,T,SSMIN,SSMAX,NSLPPT,KTER1,KTER2)
300      WRITE(7,55) $CALL GETNUM(A) $IF(A(1).EQ.0.)GOTO100
301      KTER1=10H CIP-SLIP $KTER2=10H
302      CALL AGRAPH(DIPSLP,T,DSMIN,DSMAX,NSLPPT,KTER1,KTER2)
303      WRITE(7,55) $CALL GETNUM(A) $IF(A(1).EQ.0.)GOTO100
304      68 KTER1=10HTILT AMPLI $KTER2=10HTUDE
305      CALL AGRAPH(TAMP,T,TAMPMN,TAMPMX,NRECEPT,KTER1,KTER2)
306      WRITE(7,55) $CALL GETNUM(A) $IF(A(1).EQ.0.)GOTO100
307      KTER1=10HTILT AZIMU $KTER2=10HTH
308      CALL AGRAPH(TAZM,T,TAZMMN,TAZMMX,NRECEPT,KTER1,KTER2)
309      WRITE(7,55) $CALL GETNUM(A) $IF(A(1).EQ.0.)GOTC100
310      KTER1=10HCORNER 1 $KTER2=10H
311      CALL AMINMX(CORNRI,NRECEPT,CMIN,CMAX)
312      CALL AGRAPH(CORNRI,T,CMIN,CMAX,NRECEPT,KTER1,KTER2)
313      KTER1=10HCORNER 2
314      CALL AMINMX(CORNRI,NRECEPT,CMIN,CMAX)
315      CALL AGRAPH(CORNRI,T,CMIN,CMAX,NRECEPT,KTER1,KTER2)
316      WRITE(7,55) $CALL GETNUM(A) $IF(A(1).EQ.0.)GOTO100
317      KTER1=10H STRIKE-SLI $KTER2=10HP AREA
318      CALL AMINMX(SSAREA,NRECEPT,CMIN,CMAX)
319      CALL AGRAPH(SSAREA,T,CMIN,CMAX,NRECEPT,KTER1,KTER2)
320      KTER1=10HDIP-SLIP A $KTER2=10HREA
321      CALL AMINMX(OSAREA,NRECEPT,CMIN,CMAX)
322      CALL AGRAPH(OSAREA,T,CMIN,CMAX,NRECEPT,KTER1,KTER2)
323      WRITE(7,55) $CALL GETNUM(A) $IF(A(1).EQ.0.)GOTO100
324      100 WRITE(7,93)(C(I),I=1,36)
325      93 FORMAT(6(6F10.3,/))
326      WRITE(7,115)(ICRNR(I),I=1,16)
327      WRITE(7,117)(IT(I),I=1,4),ITIME
328      WRITE(7,117)KFLAGS,KFLAGD,LFLAG,MFLAG,IFLAG
329      WRITE(7,117)NRECEPT,N,N1,N2,N3
330      115 FORMAT(2(8I6,/))
331      117 FFORMAT(5I10)
332      WRITE(7,66) $CALL GETNUM(A)
333      66 FORMAT(*1=RE-START WITH ALL NEW VALUES*,/,
334           1      *2=RE-START WITH NEW STRIKE-SLIP VALUE AND ZONE COORDINATES*,/,
335           1      *3=RE-START WITH NEW DIP-SLIP VALUE AND ZONE COORDINATES*,/,
336           1      *4=RE-START WITH NEW STRIKE-SLIP VALUE ONLY*,/,
337           1      *5=RE-START WITH NEW DIP-SLIP VALUE ONLY*,/,
338           1      *6=RE-START WITH NEW TILTMETER COORDINATES ONLY*,/,
339           1      *7=STOP*)
340      IF(A(1).EQ.1.)GOTC67 $IF(A(1).EQ.2.)GOTO62
341      IF(A(1).EQ.3.)GOT076 $IF(A(1).EQ.4.)GOT070
342      IF(A(1).EQ.5.)GOTC071 $IF(A(1).EQ.6.)GOT072
343      IF(A(1).EQ.7.)GOT073 $GOT067
344      62 WRITE(7,74)
345      74 FORMAT(*U1IN, U1FN*)
346      CALL GETNUM(A) $C(33)=A(1) $C(34)=A(2)
347      WRITE(7,15) $CALL GETNUM(A)
348      C(17)=C(19)=A(1) $C(18)=C(24)=A(2) $C(20)=C(22)=A(3)

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349      C(21)=C(23)=A(+)  $C(25)=C(27)=A(5)  $C(26)=C(32)=A(6)
350      C(28)=C(30)=A(7)  $C(29)=C(31)=A(8)  $WRITE(7,3)
351      CALL GETNUM(A)  $LFLAG=A(1)  $MFLAG=A(2)
352      DO 85 I=1,8
353      85 ICRNR(I)=1
354      IF(LFLAG.EQ.0.OR.MFLAG.EQ.0)CALL SLPCKN(LFLAG,MFLAG,ICRNR)
355      IF(LFLAG.EQ.2)GOTO 86  $GOT087
356      86 DO 88 I=9,16
357      88 ICRNR(I)=2
358      87 IF(MFLAG.EQ.2)GOTO89  $GOT090
359      89 DU 91 I=1,8
360      91 ICRNR(I)=2
361      90 GOTO75
362      76 WRITE(7,77)
363      77 FFORMAT(*U3IN, USFN*)
364      CALL GETNUM(A)  $C(35)=A(1)  $C(36)=A(2)
365      WRITE(7,17)  $CALL GETNUM(A)
366      C(1)=C(3)=A(1)  $C(2)=C(8)=A(2)
367      C(4)=C(6)=A(3)  $C(5)=C(7)=A(4)  $C(9)=C(11)=A(5)
368      C(10)=C(12)=A(6)  $C(12)=C(14)=A(7)  $C(13)=C(15)=A(8)
369      WRITE(7,3)  $CALL GETNUM(A)  $LFLAG=A(1)  $MFLAG=A(2)
370      DU 78 I=1,8
371      78 ICFNR(I)=1
372      IF(LFLAG.EQ.0.OR.MFLAG.EQ.0)CALL SLPCKN(LFLAG,MFLAG,ICRNR)
373      IF(LFLAG.EQ.2)GOTO79  $GOT080
374      79 DU 81 I=9,16
375      81 ICRNR(I)=2
376      82 IF(MFLAG.EQ.2)GOTO82  $GOT083
377      82 DU 84 I=1,8
378      84 ICRNR(I)=2
379      83 GOTO75
380      70 WRITE(7,74)  $CALL GETNUM(A)  $C(33)=A(1)  $C(34)=A(2)  $GOT075
381      71 WRITE(7,77)  $CALL GETNUM(A)  $C(35)=A(1)  $C(36)=A(2)
382      GOT075
383      72 WRITE(7,18)  $CALL GETNUM(A)  $X1=A(1)  $X2=A(2)
384      GOTO75
385      73 STOP $END
386      SUBROUTINE XPNSHL(P,Q,R1,S1,T,Y)
387      S=(T-R1)*E.  $R=S1-R1  $IF(R.EQ.0.)R=1.E-20 $ALPHA=-S/R
388      Y=((Q-P)*(1.-EXP(ALPHA)))+P
389      RETURN $END
390      SUBROUTINE ALINAR(P,Q,R,S,T,Y)
391      Y=((Q-P)*(T-R))/(S-R) + P
392      RETURN $END
393      SUBROUTINE SLPCKN(LFLAG,MFLAG,ICRNR)
394      DIMENSION A(20),ICRNR(16)
395      WRITE(7,1)
396      1 FFORMAT(*1=VARIABLE INCREMENTED EXPONENTIALLY*,/,,
397      1 *2=VARIABLE INCREMENTED LINEARLY*)
398      IF(MFLAG.NE.0)GOTO2
399      WRITE(7,3)  $CALL GETNUM(A)  $ICRNR(1)=ICRNR(3)=A(1)
400      3 FFORMAT(*D1X1, D1X3, D2X3, D3X1*)
401      ICRNR(2)=ICRNR(3)=A(2)  $ICRNR(4)=ICRNR(6)=A(3)
402      ICRNR(5)=ICRNR(7)=A(4)
403      2 IF(LFLAG.NE.0)RETURN
404      WRITE(7,4)  $CALL GETNUM(A)  $ICRNR(9)=ICRNR(11)=A(1)
405      4 FFORMAT(*C1X1, C1X3, C2X3, C3X1*)
406      ICFNR(10)=ICRNR(16)=A(2)  $ICRNR(12)=ICRNR(14)=A(3)

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407      ICRNR(13)=ICRNR(15)=A(4) $RETURN $END
408      SUBROUTINE TRIGGR(IT)
409      DIMENSION A(20),IT(4)
410      WRITE(7,1) $CALL GETNUM(A) $IT(1)=A(1) $WRITE(7,2)
411      1 FORMAT(*0 = D(I1) > C(I2), 1 = D(I1) < C(I2)*)
412      2 FORMAT(*0 = STRIKE-SLIP/1 = DIP-SLIP ZONE TRIGGERED*)
413      CALL GETNUM(A) $IT(2)=A(1) $WRITE(7,3)
414      3 FORMAT(*SPECIFY I1 AND I2*)
415      CALL GETNUM(A) $IT(3)=A(1) $IT(4)=A(2)
416      RETURN $END
417      SUBROUTINE AGRAPH(R,T,A1,B,NRECPT,K1,K2)
418      COMMON/JPLCT/XLT,XRT,YLO,YUP,MAJX,MAJY,KX(2),KY(2),
419      1 LTITL(8),LU,LTF,LNLGX,LNLGY,NCLX,NCLY,LTITL2(8)
420      DIMENSION R(50),T(50),A(20),KX(2),KY(2)
421      KX(1)=10HTIME-ARBIT $KX(2)=10HRARY UNITS
422      XLT=T(1) $XRT=T(NRECPT) $KY(1)=K1 $KY(2)=K2
423      YLC=A1 $YUP=B
424      13 WRITE(7,3) $READ(7,4)CH $IF(CH.EQ.1HN.OR.CH.EQ.1H )GOT05
425      3 FORMAT(*SET HORIZONTAL SCALE? Y OR N(=BLANK)*)
426      4 FORMAT(A1)
427      WRITE(7,6) $CALL GETNUM(A) $XLT=A(1) $XRT=A(2)
428      6 FORMAT(*MIN/MAX X VALUES*)
429      5 WRITE(7,7) $READ(7,4)CH $IF(CH.EQ.1HN.OR.CH.EQ.1H )GOT08
430      WRITE(7,9) $CALL GETNUM(A) $YLO=A(1) $YUP=A(2)
431      7 FORMAT(*SET VERTICAL SCALE? Y OR N(=BLANK)*)
432      9 FORMAT(*MIN/MAX Y VALUES*)
433      8 AA=YUP $IF(YLO.EQ.AA)YUP=YUP+1. $IF(YLO.EQ.AA)YLC=YLO-1.
434      WRITE(7,10)KY(1),KY(2)
435      10 FFORMAT(*SKJP PLCT (F *,2A10,*?*)
436      READ(7,4)IJVAR
437      IF(IJVAR.EQ.1HN.OR.IJVAR.EQ.1H )CALL PLOTS(R,T,1,NRECPT)
438      WRITE(7,12) $CALL GETNUM(A) $IRS=A(1) $IF(IRS.EQ.1)GOT013
439      12 FORMAT(*1 = NEW PLCT, 2 = RETURN*)
440      RETURN $END
441      SUBROUTINE AMINMX(F,NRECPT,B,A)
442      DIMENSION R(50)
443      AMIOPT=(R(NRECPT)-R(1))/2. + R(1)
444      A = B = AMIOPT
445      DO 1 I=1,NRECPT
446      IF(R(I).GT.A)A=R(I)
447      IF(R(I).LT.B)B=R(I)
448      1 CONTINUE
449      RETURN $END
450      SUBROUTINE CMPTLT(C,X1,X2,X3,T1,T2)
451      DIMENSION D(20)
452      A1=A2=A3=A4=B1=B2=B3=B4=0.
453      DA1=DA2=DA3=DA4=DB1=DB2=DB3=DB4=0.
454      U1=D(17) $U3=D(18)
455      IF(U1.EQ.0.)GO TO 1
456      CALL TILT(D(17),X1,X2,X3,D(11),D(12),A1,B1)
457      CALL TILT(D(17),X1,X2,X3,D(9),D(10),A2,B2)
458      CALL TILT(D(17),X1,X2,X3,D(13),D(14),A3,B3)
459      CALL TILT(D(17),X1,X2,X3,D(15),D(16),A4,B4)
460      1 IF(U3.EQ.0.)GO TO 2
461      CALL DPSPTL(D(18),X1,X2,X3,D(3),D(4),DA1,DB1)
462      CALL DPSPTL(D(18),X1,X2,X3,D(1),D(2),DA2,DB2)
463      CALL DPSPTL(D(18),X1,X2,X3,D(5),D(6),DA3,DB3)
464      CALL DPSPTL(D(18),X1,X2,X3,D(7),D(8),DA4,DB4)

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465      2 T1=A1-A2-A3+A4+DA1-DA2-DA3+DA4
466      T2=B1-B2-B3+B4+DB1-DB2-CB3+DB4
467      RETURN $END
468      SUBROUTINE TILT(U1,X1,X2,X3,P1,P3,T1,T2)
469      R=SQRT((X1-P1)**2+X2**2+(X3-P3)**2)
470      RP=R+P3
471      T1=(U1/12.5664)*(X2*(X1-P1)*(R*RP-(R+2.*P3)*(2.*R+P3)))/
472      (R**3*RP**2)
473      T2=(U1/12.5664)*(X2**2*(R*RP-(R+2.*P3)*(2.*R+P3))/(R**3*RP**2)
474      1 +(R+2.*P3)/(R*RP))
475      RETURN $END
476      SUBROUTINE DPSPTL(U3,X1,X2,X3,P1,P3,DT1,DT2)
477      R=SQRT(((X1-P1)**2)+(X2**2)+(X3-P3)**2)
478      UT1=(U3/E.28318)*((X2*P3)/R)*((1./(R**2))-(1./(((X1-P1)
479      1 **2)+(X2**2))))
480      UT2=(U3/E.28318)*(((X1-F1)*P3)/((X2**2)+(P3**2)))*(((P3**2)
481      1 -(X2**2))/(R*((X2**2)+(P3**2)))+(((X1-P1)**2)+(P3**2))
482      1 /(R**3))+((X2**2)+(P3**2))/(R*((X1-P1)**2)+(X2**2)))
483      RETURN $END
484      SUBROUTINE GETNUM(R)
485      DIMENSION R(1),L(80)
486      RLAU(7,9)L $ I=J=0
487      c J=J+1 $ N=P=S=0 $ M=F=1
488      5 I=I+1 $ IF(I.GT.80)RETURN $ D=L(I) $ K=4
489      IF(D.EQ.38)K=2 $ IF(D.GE.27.A.D.LE.36)K=1
490      IF(D.EQ.+7)K=3 $ K=K+S I GOTO(1,2,3,5,1,4,3,4)K
491      1 N=N*10+D-27           S=4          GOTO 5
492      2 M=-1                  S=4          GOTO 5
493      3 P=I                  S=4          GOTO 5
494      4 IF(P.NE.0)F=10.**(I-P-1) $ R(J)=N/F*M $ GOTO 6
495      9 FFORMAT(80R1)
496      END

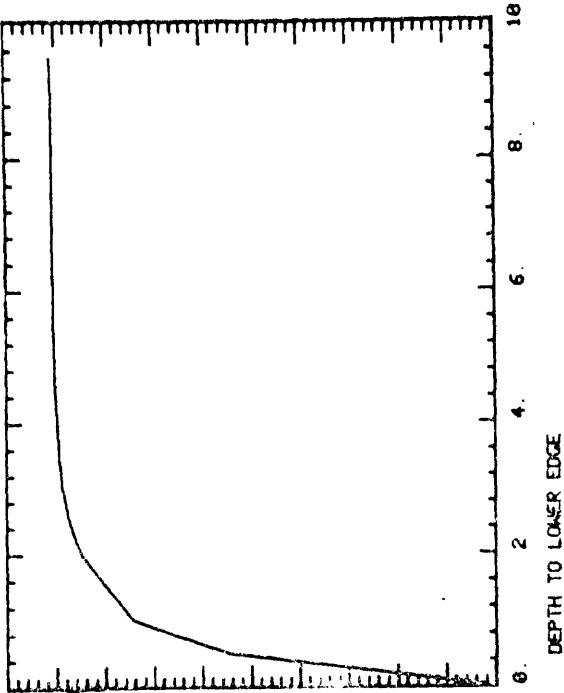
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EXAMPLE OF STRTCH

RUN!
 1=ZONE EXPANDS, 2-ZONE CONTRACTS
 1!
 1/2-SLIP INCREMENTED EXPONENTIALLY/LINEARLY
 STRIKE-SLIP/DIP-SLIP
 1.
 0 = INCREMENT CORNERS SEPARATELY
 1/2=INCREMENT ALL CORNERS EXPONENTIALLY/LINEARLY
 STRIKE-SLIP/DIP-SLIP
 1.
 U1% = LEFT-LATERAL STRIKE-SLIP
 U3% = X2>X0' SIDE DOWN
 U1IN, U1FN, U3IN, U3FN
 -1 -1 0!
 'TRIGGER' OPTION DESIRED?
 N!
 C1X1IN, C1X2IN, C2X1IN, C3X1IN, C1X1FN, C1X2FN, C2X1FN
 0 0 0 2 0 1 0!
 ENTER STATION COORDINATES-(X1,X2)
 1 .5

! WRITE PLOT TITLE, 80 CHARACTERS
 ! PROGRAM STRETCH-STRIKE-SLIP = -1 MPH
 ! MIN/MAX VALUES OF TILT AMPLITUDE = 0
 ! SET HORIZONTAL SCALE? Y OR N=BLANK,
 \\
 Y!
 ! MIN/MAX X VALUES
 ! 0 18!
 ! SET VERTICAL SCALE? Y OR N=BLANK,
 Y!
 ! MIN/MAX Y VALUES
 ! 0 .1!
 ! SKIP PLOT OF TILT AMPLITUDE ?

PROGRAM STRIKE-SLIP = -1 MM.
MAXIMUM TILT AMPLITUDE

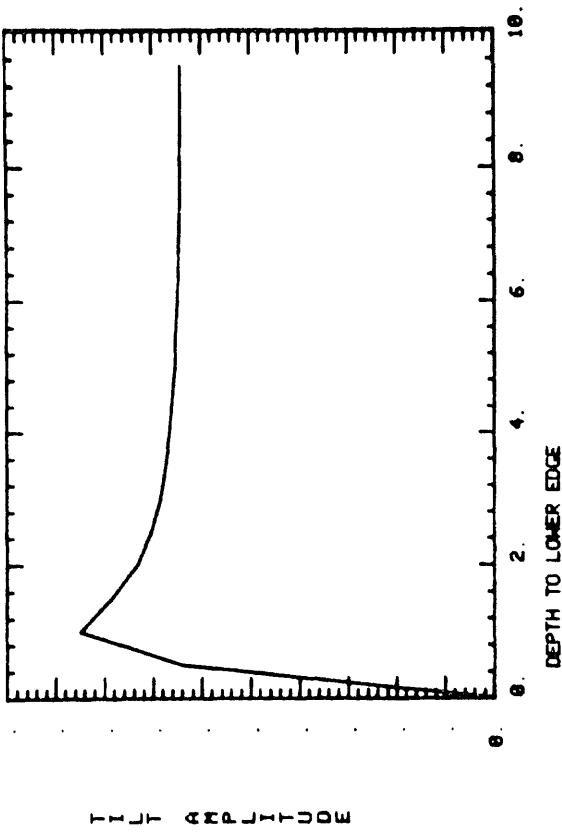


1 = NEW PLOT, 2 = RETURN
2
0=RE-START, 1=SPECIFY NEW DELTAX AND CONTINUE
0!
1=ZONE EXPANDS, 2=ZONE CONTRACTS
1!
1/2=SLIP INCREMENTED EXPONENTIALLY/LINEARLY
STRIKE-SLIP/DIP-SLIP
1.1!
0 =INCREMENT CORNERS SEPARATELY
1/2=INCREMENT ALL CORNERS EXPONENTIALLY/LINEARLY
STRIKE-SLIP/DIP-SLIP
1.1!
.U1>X0 = LEFT-LATERAL STRIKE-SLIP
.U3>X0 = 'X2>0' SIDE DOWN
U1IN, U1FN, U3IN, U3FN
0 0 1 1!
TRIGGER? OPTION DESIRED?
N
DIX1IN,DIX3IN,D2X3IN,D3X1IN,DIX1FP,DIX3FP,D2X2FP,D3X1FN
0 6 8 8 2 8 1 0!
ENTER STATION COORDINATES--(X1,X2)
1 5

2-75

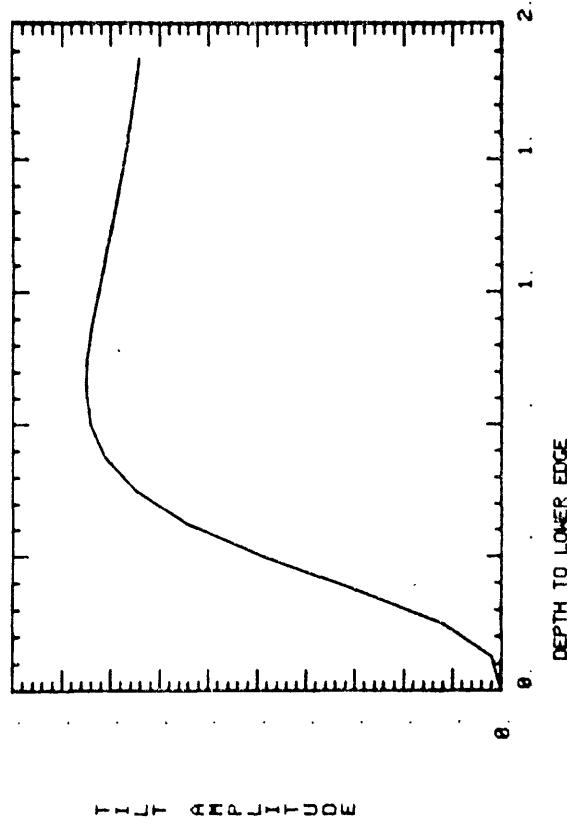
```
! WRITE PLOT TITLE, 86 CHARACTERS
! PROGRAM STRETCH-DIP-SLIP = 1 MM
! MINMAX VALUES OF TILT AMPLITUDE = 0
! SET HORIZONTAL SCALE? Y OR N <BLANK>
Y!
MINMAX X VALUES
9 16
SET VERTICAL SCALE? Y OR N <BLANK>
Y!
MINMAX Y VALUES
6 5
SKIP PLOT OF TILT AMPLITUDE ?
```

PROGRAM STRETCH-DIP-SLIP = 1 MM
MAXIMUM TILT AMPLITUDE



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PROGRAM STRETCH-DIP-SLIP=1 MM., DELTAX=.1
MAXIMUM TILT AMPLITUDE



DEPTH TO LOWER EDGE

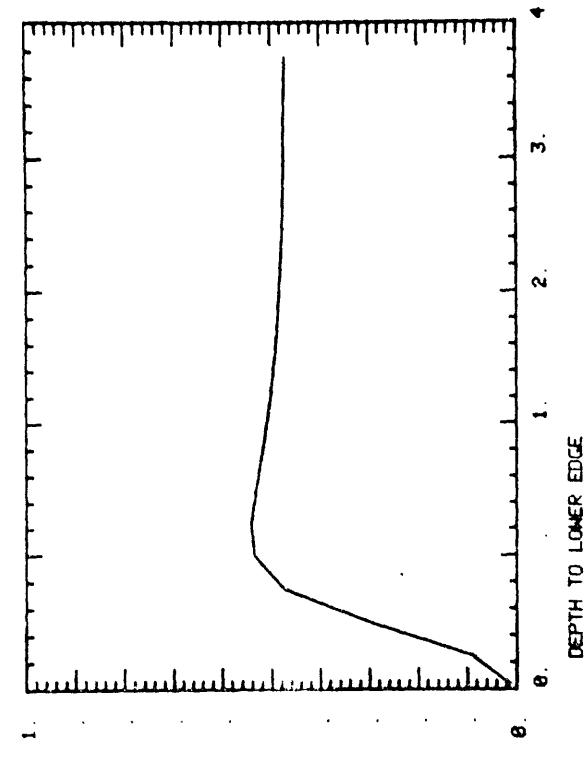
```

1 = NEW PLOT, 2 = RETURN
2
0-FE-START, 1-SPECIFY NEW DELTAX AND CONTINUE
1
ENTER NEW DELTAX
1
0-FE-START WITH ALL NEW VALUES
1-FE-START WITH PREVIOUS VALUES AND NEW DELTAX
1
WRITE PLOT TITLE, 80 CHARACTERS
PROGRAM STRETCH-DIP-SLIP=1 MM., DELTAX=.1
MIN MAX VALUES OF TILT AMPLITUDE = 9. 4.255E-01
SET HORIZONTAL SCALE? Y OR N <BLANK>
Y
HLP/PICK X VALUES
E 2
SET VERTICES SO LEFT Y OR N <BLANK>
Y
MIN MAX Y VALUES
E 5
5
GP/PLOT OF TILT AMPLITUDE ?
```

1 = NEW PLOT, 2 = RETURN
0=RE-START, 1=SPECIFY NEW DELTAX AND CONTINUE
1 ENTER NEW DELTAX
2 ENTER NEW DELTAX WITH ALL NEW VALUES
3 ENTER-START WITH PREVIOUS VALUES AND NEW DELTAX
4 ZONE EXPANDS, 2-CORE CONTRACTS
5 1/2-SLIP INCREMENTED EXPONENTIALLY LINEARLY
6 STRIKE-SLIP-DIP-SLIP
1.1 INCREMENT CORNERS SEPARATELY
6.1 INCREMENT ALL CORNERS EXPONENTIALLY LINEARLY
1.2 INCREMENT ALL CORNERS EXPONENTIALLY LINEARLY
6.2 LEFT-LATERAL STRIKE-SLIP
'U1> = 'U2> = SIDE DOWN
U1IN, U1FN, USIN, USFN
6.3 -5.0 1! TRIGGER: OPTION DESIRED?
Y

6 = $(X_{11}) > (X_{12})$, 1 = $(X_{11}) < (X_{12})$
0 = STRIKE-SLIP/1 = DIP-SLIP ZONE TRIGGERED
ENTER X1 AND X2
9.5!
C1X1IN,C1X3IN,C2X3IN,C3X1IN,C1X1FN,C1X3FN,C2X3FN
6 6 6 6 2 6 1 6!
D1X1IN,D1X3IN,D2X3IN,D3X1IN,D1X1FN,D1X3FN,D2X3FN,D3X1FN
5 6 6 5 1.5 6 1 5!
ENTER STATION COORDINATES—(X1, X2)
1.5!
PROGRAM SHUTS OFF STRIKE-SLIP AND DIP-SLIP!
WRITE PLOT TITLE, 60 CHARACTERS
MIN-X VALUES OF TILT AMPLITUDE = 0.
MIN-X VALUES OF DEPTH = 0.
SET HORIZONTAL SCROLL? Y OR N=BLANK
Y!
MINMAX X VALUES
6 4!
SET VERTICAL SCROLL? Y OR N=BLANK
Y!
MINMAX Y VALUES
6 1!
SKIP PLOT OF TILT AMPLITUDE ?

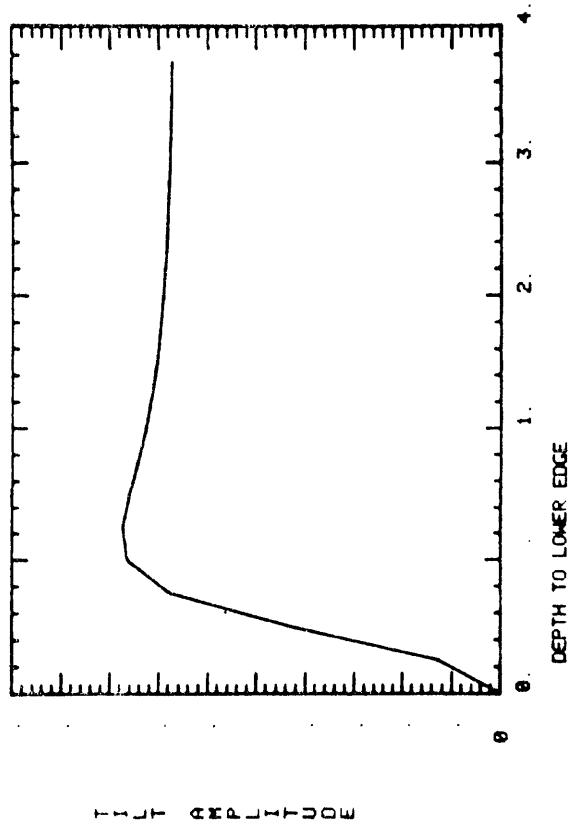
PROGRAM STRETCH/STRIKE-SLIP AND DIP-SLIP
MAXIMUM TILT AMPLITUDE



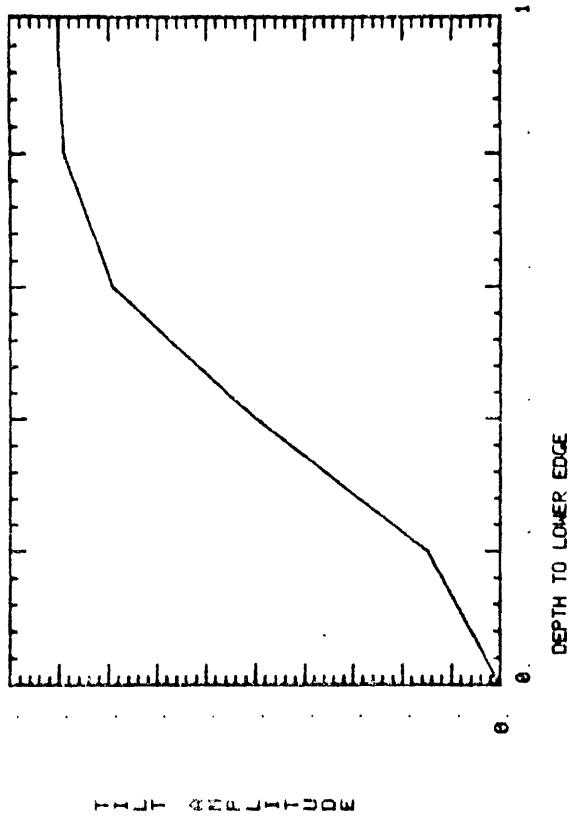
1 = NEW PLOT, 2 = RETURN
1.
SET HORIZONTAL SCALE? Y OR N >BLANK>
Y
MIN MAX X VALUES
0 4
SET VERTICAL SCALE? Y OR N >BLANK>
Y
MIN MAX Y VALUES
0 7
SKIP PLOT OF TILT AMPLITUDE ?

PROGRAM STRETCH-STRIKE-SLIP AND DIP-SLIP
MAXIMUM TILT AMPLITUDE

```
1 = NEW PLOT, 2 = RETURN  
1  
SET HORIZONTAL SCALE? Y OR N=BLANK  
Y  
MIN-MAX X VALUES  
0 1  
SET VERTICAL SCALE? Y OR N=BLANK  
Y  
MIN-MAX Y VALUES  
0 6  
SKIP PLOT OF TILT AMPLITUDE ?
```

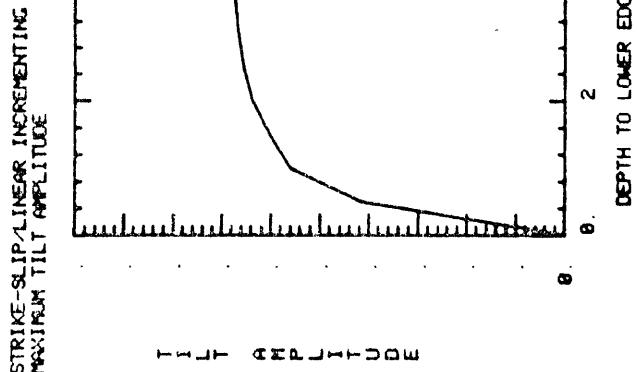


PROGRAM STRETCH-STRIKE-SLIP AND DIP-SLIP
MAXIMUM TILT AMPLITUDE



1 = NEW PLOT, 2 = RETURN
2
0=RE-START, 1=SPECIFY NEW DELTAX AND CONTINUE
ENTER NEW DELTAX
5
0=RE-START WITH ALL NEW VALUES
1=RE-START WITH PREVIOUS VALUES AND NEW DELTAX
0

1=ZONE EXPANDS, 2=ZONE CONTRACTS
 1/2=SLIP INCREMENTED EXPONENTIALLY/LINEARLY
 STRIKE-SLIP DIP-SLIP
 2 21
 8 =INCREMENT CORNERS SEPARATELY
 1/2=INCREMENT ALL CORNERS EXPONENTIALLY/LINEARLY
 STRIKE-SLIP DIP-SLIP
 2 21
 11:30: LEFT-LATERAL STRIKE-SLIP
 U3 > 3 : X2 > 0 : SIDE DOWN
 U1FN, U1FN, U2IH, U2FN
 -3 -3 6 6!
 'TRIGGER' OPTION DESIRED?
 N
 C1X1FN, C1X3FN, C2X1FN, C2X3FN, C3X1FN
 0 0 0 2 0 1 6!
 ENTER STATION COORDINATES—(X1,X2)
 1 .5!
 WRITE PLOT TITLE, 80 CHARACTERS
 STRIKE-SLIP/LINEAR INC
 MIN/MAX VALUES OF TILT AMPLITUDE = 0.
 MIN/MAX VALUES OF DEPTH = 0.
 SET HORIZONTAL SCALE? Y OR N =BLANK
 Y!
 MIN/MAX X VALUES
 6 10!
 SET VERTICAL SCALE? Y OR N =BLANK
 Y!
 MIN/MAX Y VALUES
 0 4!
 SKIP PLOT OF TILT AMPLITUDE ?
 ?

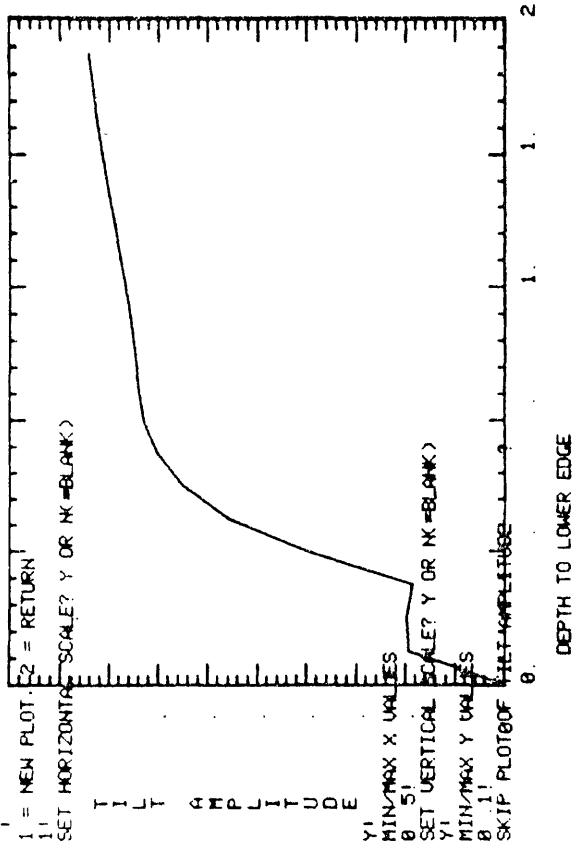


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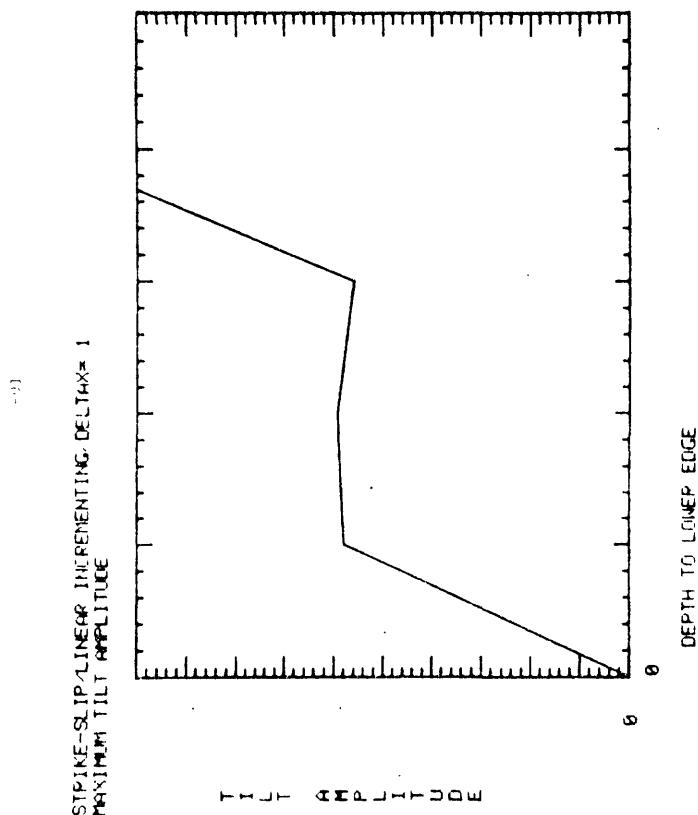
1 - NEW PLOT, 2 = RETURN
2 - RE-START, 1=SPECIFY NEW DELTAX AND CONTINUE
ENTER NEW DELTAX
1.
0.0E+00 START WITH ALL NEW VALUES
1 - RE-START WITH PREVIOUS VALUES AND NEW DELTAX
1.
WRITE PLOT TITLE, 80 CHARACTERS
STRIKE-SLIP/LINEAR INCREMENTING/DELTAX= 1
MIN-MAX VALUES OF TILT AMPLITUDE = 0.
2.526E-01
1.968E+00
MIN-MAX VALUES OF DEPTH = 6.
SET HORIZONTAL SCALE? Y OR N =BLANK?
YI
MIN-MAX X VALUES
6.21
SET VERTICAL SCALE? Y OR N =BLANK?
YI
MIN-MAX Y VALUES
6.31
SKIP PLOT OF TILT AMPLITUDE ?

```

STRIKE-SLIP/LINEAR INCREMENTING/DELTAX= 1
MIN-MAX TILT AMPLITUDE



1 - NEW PLOT, 2 - RETURN
1 - RE-START, 2 - SPECIFY NEW DELTA X AND CONTINUE
2 - ~EDIT



PROGRAM LISTING FOR STRTCH

07 JUL 76 08.37.44 MCHUGH .STRTCH

```

1  DELETE(LGO,OUTFUT,STRTCH)
2  STRTCH.
3  CXIT.
4  LIBCOPY(GRAPHIC,TXLGO/RR,TXLGO)
5  LIBCOPY(JDRAT,NPLGO/RR,NPLGO)
6  DELETE(LGO,OUTPUT,STRTCH)
7  RUN76(S)
8  LINK(F=LGO,F=TXLGO,F=NPLGO,B=STRTCH)
9  STRTCH.
10 FIN.
11 EOR
12      PROGRAM STRTCH(TAPEPTY=201,FILM=TAPE TTY,TAPE7=TAPEPTY)
13      CCOMMON/T VPCOL/TVPUL(8)
14      COMMON/TVTUNE/ITUNE(30)
15      CCOMMON/JPLCT/XLT,XRT,YLO,YUP,MAJX,MAJY,KX(2),KY(2),
16      LTITLE(8),LU,LTF,LNLGX,LNLGY,NCLX,NCLY,LTITLE2(8)
17      DIMENSION IFET(8)
18      DIMENSION TX(50),TY(50),T(50)
19      DIMENSION C(20),C(40),A(30),IT(4),ICRNR(16)
20      DIMENSION AMPMAX(50),DEPTH(50)
21      DIMENSION THETA1(50,50),THETA2(50,50)
22      DIMENSION TAMP(50),TAZM(50)
23      CALL FET(5LTAP7,IFET,8)
24      IFET(2)=IFET(2).OR.0.0000 0010 0000 0000 0000B
25      IFET(8)=IFET(8).OR.4.000 0000 0000 0000 0000B
26      CALL FET(5LTAP7,IFET,-8)
27      KTEST=1 $DELTA=5 $CASE=-DELTAX
28      DO 101 J=1,18
29      D(J)=0. $C(J+18)=0. $C(J)=0.
30 101 CONTINUE
31      WRITE(7,1)
32      1  FFORMAT(*1=ZONE EXPANDS, 2=ZONE CONTRACTS*)
33      CALL GETNUM(A) $IFLAG=A(1) $WRITE(7,2)
34      2  FORMAT(*1/2=SLIP INCREMENTED EXPONENTIALLY/LINEARLY*,/,
35      1      *STRIKE-SLIP/DIF-SLIP*)
36      CALL GETNUM(A) $KFLAG=A(1) $KFLAG=A(2) $WRITE(7,3)
37      3  FORMAT(*0 =INCREMENT CORNERS SEPARATELY*,/,
38      1      *1/2=INCREMENT ALL CORNERS EXPONENTIALLY/LINEARLY*,/,
39      1      *STRIKE-SLIP/DIF-SLIP*)
40      CALL GETNUM(A) $LFLAG=A(1) $MFLAG=A(2)
41      DO 110 I=1,4
42      IT(I)=5
43 110 CONTINUE
44      DO 4 I=1,1E
45      4  ICRNR(I)=1
46      IF(LFLAG.EQ.0.OR.MFLAG.EQ.0)CALL SLPCRM(LFLAG,MFLAG,ICRNR)
47      IF(LFLAG.EQ.2)GOTO 5 $GOTO6
48      5  DO 7 I=9,1E
49      7  ICRNR(I)=2
50      6  IF(MFLAG.EQ.2)GOTO8 $GOTO9
51      8  DO 10 I=1,8
52      10 ICRNR(I)=2
53      9  WRITE(7,11) $CALL GETNUM(A) $C(33)=A(1) $C(34)=A(2)
54      11  FORMAT(*'U1>0' = LEFT-LATERAL STRIKE-SLIP*,/,
55      1      *'U3>0' = 'X2>0' SIDE DOWN*,/,
56      1      *U1IN, U1FN, U3IN, U3FN*)
57      1  C(35)=A(3) $C(36)=A(4) $WRITE(7,12)
58      12 FFORMAT(*'TRIGGER' OPTION DESIRED?*)

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59      READ(7,13)TRIG $IF(TRIG.EQ.1HY)CALL TRIGGR(IT)
60      13 FORMAT(A1)
61      IF(C(33).EQ.0..AND.C(34).EQ.0.)GOTO14
62      WRITE(7,15) $CALL GETNUM(A) $C(17)=C(19)=A(1)
63      15 FORMAT(*C1X1IN,C1X3IN,C2X3IN,C3X1IN,C1X1FN,C1X3FN,C2X3FN,C3X1FN*)
64      C(18)=C(24)=A(2) $C(20)=C(22)=A(3) $C(21)=C(23)=A(4)
65      C(25)=C(27)=A(5) $C(26)=C(32)=A(6) $C(28)=C(30)=A(7)
66      C(29)=C(31)=A(8)
67      14 IF(C(35).EQ.0..AND.C(36).EQ.0.)GOTO16
68      WRITE(7,17) $CALL GETNUM(A) $C(1)=C(3)=A(1) $C(2)=C(8)=A(2)
69      17 FORMAT(*D1X1IN,D1X3IN,D2X3IN,D3X1IN,D1X1FN,D1X3FN,D2X3FN,D3X1FN*)
70      C(4)=C(6)=A(3) $C(5)=C(7)=A(4) $C(9)=C(11)=A(5)
71      C(10)=C(16)=A(6) $C(12)=C(14)=A(7) $C(13)=C(15)=A(8)
72      16 WRITE(7,18) $CALL GETNUM(A) $X1=A(1) $X2=A(2)
73      18 FORMAT(*ENTER STATION COORDINATES--(X1,X2)*)
74      X3=0. $NRECPT=50 $N=(.075*NRECPT) $NSLPPT=NRECPT
75      N1=N+1 $N2=NRECPT-(.075*NRECPT)-1
76      N3=N2+1 $PI=3.1415926 $DEPTHL=CASE
77      RNSLPP=NSLPPT $RN1=N1 $RN2=Y2 $ONE=1. $ITIME=99999
78      75 CONTINUE
79      DEPTHL=DEPTHL+DELTAX $C(28)=DEPTHL $C(20)=C(22)=C(30)=C(28)
80      C(4)=C(12)=C(6)=C(14)=C(28)
81      DO 21 J=1,8
82      D(J)=C(J) $D(J+8)=C(J+16)
83      21 CONTINUE
84      J(17)=C(33) $D(18)=C(35)
85      DO 19 I=1,N
86      T(I)=I
87      DO 63 K=1,NSLPPT
88      CALL CMPTLT(D,X1,X2,X3,T1,T2)
89      THETA1(I,K)=T1 $THETA2(I,K)=T2
90      63 CONTINUE
91      19 CONTINUE
92      DO 24 J=1,8
93      D(J)=C(J+8) $D(J+8)=C(J+24)
94      24 CONTINUE
95      C(17)=C(34) $D(18)=C(36)
96      DO 23 I=N3,NRECPT
97      T(I)=I
98      DO 64 K=1,NSLPPT
99      RK=K $CALL XPNSHL(C(33),C(34),ONE,RNSLPP,RK,Y1)
100     CALL XPNSHL(C(35),C(36),ONE,RNSLPP,RK,Y2)
101     IF(KFLAGS.NE.1)CALL ALINAR(C(33),C(34),ONE,RNSLPP,FK,Y1)
102     IF(KFLAGS.NE.1)CALL ALINAR(C(35),C(36),ONE,RNSLPP,FK,Y2)
103     D(17)=Y1 $D(18)=Y2
104     CALL CMPTLT(D,X1,X2,X3,T1,T2)
105     THETA1(I,K)=T1 $THETA2(I,K)=T2
106     64 CONTINUE
107     23 CONTINUE
108     IFGREC=0
109     DO 25 I=N1,N2
110     T(I)=I $RI=I
111     DO 65 K=1,NSLPPT
112     RK=K
113     IF(TRIG.EQ.1HY)GOTO26
114     DO 27 J=1,8
115     J8=J+8 $A1=C(J) $B=C(J8) $E=C(J8+8) $F=C(J+24)
116     CALL XPNSHL(A1,B,RN1,RN2,RI,Y1)

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117      CALL XPNSHL(E,F,RN1,RN2,RI,Y2)
118      IF(ICRNR(J).EQ.2)CALL ALINAR(A1,B,RN1,RN2,FI,Y1)
119      IF(ICRNR(J8).EQ.2)CALL ALINAR(E,F,RN1,RN2,FI,Y2)
120      D(J)=Y1  $D(J8)=Y2
121
122      27 CONTINUE
123      CALL XPNSHL(C(33),C(34),ONE,RNSLPP,RK,Y1)
124      CALL XPNSHL(C(35),C(36),ONE,RNSLPP,RK,Y2)
125      IF(KFLAGS.NE.1)CALL ALINAR(C(33),C(34),ONE,RNSLPP,RK,Y1)
126      IF(KFLAGD.NE.1)CALL ALINAR(C(35),C(36),ONE,RNSLPP,RK,Y2)
127      D(17)=Y1  $D(18)=Y2  GOT028
128      26 IF(IT(2).EG.1.AND.KFLAGS.EQ.1)CALL XPNSHL(C(33),C(34),ONE,
129          1 RNSLPP,RK,Y)
130          IF(IT(2).EG.1.AND.KFLAGS.NE.1)CALL ALINAR(C(33),C(34), ONE,
131          1 RNSLPP,RK,Y)
132          IF(IT(2).EG.0.AND.KFLAGD.EQ.1)CALL XPNSHL(C(35),C(36),ONE,
133          1 RNSLPP,RK,Y)
134          IF(IT(2).EG.0.AND.KFLAGD.NE.1)CALL ALINAR(C(35),C(36),ONE,
135          1 RNSLPP,RK,Y)
136          IF(IT(2).EG.0)D(18)=Y  $IF(IT(2).EG.1)D(17)=Y
137          DO 32 J=1,8
138          J8=J+8  $A1=C(J)  $B=C(J8)  $E=C(J8+8)  $F=C(J+24)
139          CALL XPNSHL(A1,B,RN1,RN2,RI,Y1)
140          CALL XPNSHL(E,F,RN1,RN2,RI,Y2)
141          IF(ICRNR(J).EQ.2)CALL ALINAR(A1,B,RN1,RN2,FI,Y1)
142          IF(ICRNR(J8).EQ.2)CALL ALINAR(E,F,RN1,RN2,FI,Y2)
143          D(J)=Y1  $D(J8)=Y2
144          32 CONTINUE
145          MIT3=IT(3)  $MIT4=IT(4)  $IF(IT(1).EQ.1)GOTC29
146          IF(D(MIT3).LT.C(MIT4).AND.IT(2).EG.0)D(17)=C(33)
147          IF(D(MIT3).LT.C(MIT4).AND.IT(2).EQ.1)D(18)=C(35)
148          IF(D(MIT3).GE.C(MIT4))GOT033
149          DO 40 J=9,16
150          D(J)=C(J+8)
151          GOT028
152          29 IF(D(MIT3).GT.C(MIT4).AND.IT(2).EQ.0)D(17)=C(33)
153          IF(D(MIT3).GT.C(MIT4).AND.IT(2).EG.1)D(18)=C(35)
154          IF(D(MIT3).GT.C(MIT4).AND.IT(2).EQ.1)GOT033
155          IF(D(MIT3).LE.C(MIT4))GOT035
156          DO 34 J=9,16
157          34 D(J)=C(J+8)
158          GOT028
159          33 DO 36 J=1,8
160          36 D(J)=C(J)
161          GOT028
162          35 IF(IFGREC=IFGREC+1
163              IF(IFGREC.EQ.1)ITIME=I
164              IF(IFGREC.EQ.1)RITIME=ITIME
165              IF(IT(2).EG.0.AND.KFLAGS.EQ.1)CALL XPNSHL(C(33),C(34),ONE,
166                  1 RNSLPP,RK,Y)
167              IF(IT(2).EG.0.AND.KFLAGS.NE.1)CALL ALINAR(C(33),C(34),ONE,
168                  1 RNSLPP,RK,Y)
169              IF(IT(2).EG.1.AND.KFLAGD.EQ.1)CALL XPNSHL(C(35),C(36),ONE,
170                  1 RNSLPP,RK,Y)
171              IF(IT(2).EG.1.AND.KFLAGD.NE.1)CALL ALINAR(C(35),C(36),ONE,
172                  1 RNSLPP,RK,Y)
173              IF(IT(2).EG.1)D(18)=Y  $IF(IT(2).EQ.0)D(17)=Y
174              IF(IT(2).EG.1)GOT037

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175      DO 38 J=9,16
176      A1=C(J+8) $B=C(J+16) $CALL XPNSHL(A1,B,RITIME,RN2,RI,Y)
177      IF(ICRNR(J).EQ.2)CALL ALINAR(A1,B,RITIME,RN2,RI,Y)
178      38 D(J)=Y
179      GOTO28
180      37 DO 39 J=1,8
181      E=C(J) $F=C(J+8) $CALL XPNSHL(E,F,RITIME,RN2,RI,Y)
182      IF(ICRNR(J).EQ.2)CALL ALINAR(E,F,RITIME,RN2,RI,Y)
183      39 D(J)=Y
184      28 CALL CMPTLT(D,X1,X2,X3,T1,T2)
185      THETA1(I,K)=T1 $THETA2(I,K)=T2
186      65 CONTINUE
187      25 CONTINUE
188      DO 41 I=1,NRECPY
189      SUM11=SUM12=SUM21=SUM22=0.
190      DO 42 J=1,I
191      AT=THETA1(J,I+1-J) $B=THETA2(J,I+1-J) $SUM11=AT+SUM11
192      SUM21=B+SUM21
193      42 CONTINUE
194      LM=I-1 $IF(LM.LT.1)GOTO43
195      DO 44 J=1,LM
196      AT=THETA1(J,I-J) $B=THETA2(J,I-J) $SUM12=AT+SUM12 $SUM22=B+SUM22
197      44 CONTINUE
198      43 TX(I)=SUM21-SUM22 $TY(I)=SUM11-SUM12
199      41 CONTINUE
200      IF(IFLAG.EQ.2)GOTO46
201      AR=TX(1) $B=TY(1)
202      DO 47 I=1,NRECPY
203      TX(I)=TX(I)-AR
204      47 TY(I)=TY(I)-B
205      GOTO48
206      46 DO 49 I=1,NRECPY
207      TX(I)=TX(NRECPY)-TX(I)
208      49 TY(I)=TY(NRECPY)-TY(I)
209      48 CONTINUE
210      DO 50 I=1,NRECPY
211      TAMP(I)=SQRT((TX(I)**2)+(TY(I)**2))
212      50 CONTINUE
213      CALL AMINMX(TAMP,NRECPY,TAMPMN,TAMPMX)
214      AMPMAX(KTEST)=TAMPMX
215      DEPTH(KTEST)=C(28)
216      KTEST=KTEST+1
217      IF(KTEST.LE.20)GOTO75
218      KTEST=20 $DEPTHL=CASE
219      LU=7 $LNLGX=1 $LNLYG=1 $NCLX=2 $NCLY=2
220      DO 200 KM=4,8
221      200 LTITL2(KM)=10H
222      LTITL2(1)=10HMAXIMUM TI $LTITL2(2)=10HLT AMPLITU
223      LTITL2(3)=10HDL
224      WRITE(7,53) $READ(7,54)(LTITL(I),I=1,8)
225      53 FORMAT(*WRITE PLOT TITLE, 60 CHARACTERS*)
226      54 FORMAT(8A10)
227      MAJX=5 $MAJY=10
228      CALL AMINMX(AMPMAX,KTEST,A1,A2)
229      CALL AMINMX(DEPTH,KTEST,B1,B2)
230      WRITE(7,52)A1,A2,B1,B2
231      52 FORMAT(*MIN/MAX VALUES OF TILT AMPLITUDE = *,E10.3,5X,E10.3,/,,
232      1           *MIN/MAX VALUES OF DEPTH             = *,E10.3,5X,E10.3)
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233      68 KTER1=10HTILT AMPLI $KTER2=10HTUDE
234      CALL AGRAPF(AMPMAX,DEPTH,A1,A2,KTEST,KTER1,KTER2)
235      WRITE(7,1234) $CALL GETNUM(A) $IF(A(1).EQ.1.)WRITE(7,1235)
236 1234 FORMAT(*G=RE-START, 1=SPECIFY NEW DELTAX AND CONTINUE*)
237 1235 FORMAT(*ENTER NEW DELTAX*)
238      KTEST=1 $IF(A(1).EQ.0.)GOT067 $IF(A(1).EQ.1.)GOT01236
239      GOT073
240 1236 CALL GETNUM(A) $DELTAX=A(1) $DEPTHL=CASE=-DELTAX $KTEST=1
241      WRITE(7,1237) $CALL GETNUM(A) $IF(A(1).EQ.0.)GOT067
242 1237 FORMAT(*0=RE-START WITH ALL NEW VALUES*,/,,
243      1 *1=RE-START WITH PREVIOUS VALUES AND NEW [DELTAX*]
244      GOT075
245      73 STOP $END
246      SUBROUTINE XPNSHL(P,Q,R1,S1,T,Y)
247      S=(T-R1)*6. $R=S1-R1 $IF(R.EQ.0.)R=1.E-21 $ALPHA=-S/R
248      Y=((Q-P)*(1.-EXP(ALPHA)))+P
249      RETURN $END
250      SUBROUTINE ALINAR(P,Q,R,S,T,Y)
251      Y=((Q-P)*(T-R))/(S-R) + P
252      RETURN $END
253      SUBROUTINE SLPCRN(LFLAG,MFLAG,ICRNR)
254      DIMENSION A(20),ICRNF(16)
255      WRITE(7,1)
256      1 FORMAT(*1=VARIABLE INCREMENTED EXPONENTIALLY*,/,
257      1 *2=VARIABLE INCREMENTED LINEARLY*)
258      IF(MFLAG.NE.0)GOT02
259      WRITE(7,3) $CALL GETNUM(A) $ICRNR(1)=ICRNR(3)=A(1)
260      3 FORMAT(*D1X1, C1X3, D2X3, D3X1*)
261      ICRNR(2)=ICRNR(8)=A(2) $ICRNR(4)=ICRNR(6)=A(3)
262      ICRNR(5)=ICRNR(7)=A(4)
263      2 IF(LFLAG.NE.0)RETURN
264      WRITE(7,4) $CALL GETNUM(A) $ICRNR(9)=ICRNR(11)=A(1)
265      4 FORMAT(*C1X1, C1X3, C2X3, C3X1*)
266      ICRNR(10)=ICRNR(16)=A(2) $ICRNR(12)=ICRNR(14)=A(3)
267      ICRNR(13)=ICRNR(15)=A(4) $RETURN $END
268      SUBROUTINE TRIGGR(IT)
269      DIMENSION A(20),IT(4)
270      WRITE(7,1) $CALL GETNUM(A) $IT(1)=A(1) $WRITE(7,2)
271      1 FORMAT(*0 = D(I1) > C(I2), 1 = D(I1) < C(I2)*)
272      2 FORMAT(*0 = STRIKE-SLIP/1 = DIP-SLIP ZONE TRIGGERED*)
273      CALL GETNUM(A) $IT(2)=A(1) $WRITE(7,3)
274      3 FORMAT(*SPECIFY I1 AND I2*)
275      CALL GETNUM(A) $IT(3)=A(1) $IT(4)=A(2)
276      RETURN $END
277      SUBROUTINE AGRAPH(R,T,A1,B,NRECPT,K1,K2)
278      COMMON/JPLCT/XLT,XRT,YLC,YUP,MAJX,MAJY,KX(2),KY(2),
279      1 LTITL(8),LU,LTF,LNLGX,LNLGY,NCLX,NCLY,LTITL2(3)
280      DIMENSION R(50),T(50),A(20),KX(2),KY(2)
281      KX(1)=10HDEPTH TO L $KX(2)=10HOWER EDGE
282      XLT=T(1) $XRT=T(NRECPT) $KY(1)=K1 $KY(2)=K2
283      YLC=A1 $YLP=B
284      13 WRITE(7,3) $READ(7,4)CH $IF(CH.EQ.1HN.OR.CH.EQ.1H)GOT05
285      3 FORMAT(*SET HORIZONTAL SCALE? Y OR N(=BLANK)*)
286      4 FORMAT(A1)
287      WRITE(7,6) $CALL GETNUM(A) $XLT=A(1) $XRT=A(2)
288      6 FORMAT(*MIN/MAX X VALUES*)
289      5 WRITE(7,7) $READ(7,4)CH $IF(CH.EQ.1HN.OR.CH.EQ.1H)GOT08
290      WRITE(7,9) $CALL GETNUM(A) $YLO=A(1) $YUP=A(2)

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291    7 FORMAT(*SET VERTICAL SCALE? Y OR N (=BLANK)*)
292    9 FORMAT(*MIN/MAX Y VALUES*)
293    8 AA=YUP $ IF(YLO.EQ.AA)YUP=YUP+1. $ IF(YLO.EQ.AA)YLC=YLO-1.
294    WRITE(7,10)KY(1),KY(2)
295   10 FORMAT(*SKIP PLOT OF *,2A10,*??)
296    READ(7,4)IJVAR
297    IF(IJVAR.EQ.1HN.OR.IJVAR.EQ.1H )CALL PLOTS(R,T,1,NRECPT)
298    WRITE(7,12) $CALL GETNUM(A) $IRS=A(1) $IF(IRS.EQ.1)GOT013
299   12 FCRMAT(*1 = NEW PLCT, 2 = RETURN*)
300    RETURN $ENC
301    SUBROUTINE AMINMX(R,NRECPT,B,A)
302    DIMENSION F(50)
303    AMIDOPT=((R(NRECPT)-R(1))/2.) + R(1)
304    A = B = AMICPT
305    DO 1 I=1,NRECPT
306    IF(R(I).GT.A)A=R(I)
307    IF(R(I).LT.B)B=R(I)
308   1 CONTINUE
309    RETURN $ENC
310    SUBROUTINE CMPTLT(D,X1,X2,X3,T1,T2)
311    DIMENSION D(20)
312    A1=A2=A3=A4=B1=B2=B3=B4=0.
313    JA1=DA2=DA3=DA4=0B1=0B2=0B3=0B4=0.
314    U1=D(17) $U3=D(18)
315    IF(U1.EQ.0.)GO TO 1
316    CALL TILT(D(17),X1,X2,X3,D(11),D(12),A1,B1)
317    CALL TILT(D(17),X1,X2,X3,D(9),D(10),A2,B2)
318    CALL TILT(D(17),X1,X2,X3,D(13),D(14),A3,B3)
319    CALL TILT(D(17),X1,X2,X3,D(15),D(16),A4,B4)
320   1 IF(U3.EQ.0.)GO TO 2
321    CALL DPSPTL(D(18),X1,X2,X3,D(3),D(4),DA1,DE1)
322    CALL DPSPTL(D(18),X1,X2,X3,D(1),D(2),DA2,DE2)
323    CALL DPSPTL(D(18),X1,X2,X3,D(5),D(6),DA3,DE3)
324    CALL DPSPTL(D(18),X1,X2,X3,D(7),D(8),DA4,DE4)
325    2 T1=A1-A2-A3+A4+DA1-DA2-DA3+DA4
326    T2=B1-B2-B3+B4+DB1-DB2-DB3+DB4
327    RETURN $ENC
328    SUBROUTINE TILT(U1,X1,X2,X3,P1,P3,T1,T2)
329    F=SQRT((X1-P1)**2+X2**2+(X3-P3)**2)
330    RP=R+P3
331    T1=(U1/12.5664)*(X2*(X1-P1)*(R*RP-(R+2.*P3)*(2.*R+P3)))/
332    1 (R**3*RP**2)
333    T2=(U1/12.5664)*(X2**2*(R*RP-(R+2.*P3)*(2.*R+P3))/(R**3*RP**2)
334    1 +(R+2.*P3)/(F*RP))
335    RETURN $ENC
336    SUBROUTINE DPSPTL(U3,X1,X2,X3,P1,P3,DT1,DT2)
337    R=SQRT(((X1-P1)**2)+(X2**2)+((X3-P3)**2))
338    DT1=(U3/6.28318)*((X2*P3)/R)*((1./(R**2))-(1./(((X1-P1)
339    1 **2)+(X2**2))))
340    DT2=(U3/6.28318)*(((X1-P1)**2)/((X2**2)+(P3**2)))*(((P3**2)
341    1 -(X2**2))/(R*((X2**2)+(P3**2)))+(((X1-P1)**2)+(P3**2))
342    1 /(R**3))+((X2**2)+(P3**2))/(R*((((X1-P1)**2)+(X2**2))))
343    RETURN $ENC
344    SUBROUTINE GETNUM(R)
345    DIMENSION F(1),L(80)
346    READ(7,9)L $ I=J=0
347    6 J=J+1 $ N=P=S=0 $ M=F=1
348    5 I=I+1 $ IF(I.GT.80)RETURN $ D=L(I) $ K=4

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349      IF(D.EQ.38)K=2 $ IF(D.GE.27.A.D.LE.36)K=1
350      IF(D.EQ.47)K=3 $ K=K+S $ GOT0(1,2,3,5,1,4,3,4)K
351      1 N=N*10+D-27          S S=4      $ GO10 5
352      2 M=-1                S S=4      $ GO10 5
353      3 P=I                S S=4      $ GO10 5
354      4 IF(P.NE.0)F=10.**(I-P-1) $ R(J)=N/F*M $ GO10 6
355      9 FORMAT(80R1)
356      END
```